

## Normally – OFF Silicon Carbide Junction Transistor

$V_{DS}$	=	600 V
$R_{DS(ON)}$	=	60 mΩ
$I_D (T_c = 25^\circ C)$	=	32 A
$h_{FE} (T_c = 25^\circ C)$	=	80

### Features

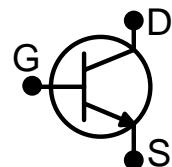
- 225°C maximum operating temperature
- Electrically Isolated Base Plate
- Gate Oxide Free SiC Switch
- Exceptional Safe Operating Area
- Excellent Gain Linearity
- Compatible with 5 V TTL Gate Drive
- Temperature Independent Switching Performance
- Low Output Capacitance
- Positive Temperature Coefficient of  $R_{DS,ON}$
- Suitable for Connecting an Anti-parallel Diode

### Advantages

- Compatible with Si MOSFET/IGBT Gate Drive ICs
- > 20 µs Short-Circuit Withstand Capability
- Lowest-in-class Conduction Losses
- High Circuit Efficiency
- Minimal Input Signal Distortion
- High Amplifier Bandwidth

### Package

- RoHS Compliant



TO – 257 (Isolated Base-plate Hermetic Package)

### Applications

- Down Hole Oil Drilling
- Geothermal Instrumentation
- Solenoid Actuators
- General Purpose High-Temperature Switching
- Amplifiers
- Solar Inverters
- Switched-Mode Power Supply (SMPS)
- Power Factor Correction (PFC)

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## Section I: Absolute Maximum Ratings

Parameter	Symbol	Conditions	Values	Unit
Drain – Source Voltage	$V_{DS}$	$V_{GS} = 0 \text{ V}$	600	V
Continuous Drain Current	$I_D$	$T_J = 225^\circ \text{C}, T_C = 25^\circ \text{C}$	32	A
Gate Peak Current	$I_{GM}$		2	A
Turn-Off Safe Operating Area	RBSOA	$T_{VJ} = 225^\circ \text{C}, I_G = 1.5 \text{ A},$ Clamped Inductive Load	$I_{D,max} = 32$ @ $V_{DS} \leq V_{DSmax}$	A
Short Circuit Safe Operating Area	SCSOA	$T_{VJ} = 225^\circ \text{C}, I_G = 1.5 \text{ A}, V_{DS} = 400 \text{ V},$ Non Repetitive	>20	µs
Reverse Gate – Source Voltage	$V_{GS}$		30	V
Reverse Drain – Source Voltage	$V_{DS}$		40	V
Power Dissipation	$P_{tot}$	$T_J = 225^\circ \text{C}, T_C = 25^\circ \text{C}$	172	W
Operating and Storage Temperature	$T_J, T_{stg}$		-55 to 225	°C

## Section II: Static Electrical Characteristics

Parameter	Symbol	Conditions	Values			Unit
			min.	typ.	max.	
<b>A: On State</b>						
Drain – Source On Resistance	$R_{DS(ON)}$	$I_D = 20 \text{ A}, T_j = 25^\circ\text{C}$ $I_D = 20 \text{ A}, T_j = 125^\circ\text{C}$ $I_D = 20 \text{ A}, T_j = 175^\circ\text{C}$ $I_D = 20 \text{ A}, T_j = 250^\circ\text{C}$	60 96 128 155			$\text{m}\Omega$
Gate – Source Saturation Voltage	$V_{GS,SAT}$	$I_D = 20 \text{ A}, I_D/I_G = 40, T_j = 25^\circ\text{C}$ $I_D = 20 \text{ A}, I_D/I_G = 30, T_j = 175^\circ\text{C}$	3.44 3.24			V
DC Current Gain	$h_{FE}$	$V_{DS} = 5 \text{ V}, I_D = 20 \text{ A}, T_j = 25^\circ\text{C}$ $V_{DS} = 5 \text{ V}, I_D = 20 \text{ A}, T_j = 125^\circ\text{C}$ $V_{DS} = 5 \text{ V}, I_D = 20 \text{ A}, T_j = 175^\circ\text{C}$ $V_{DS} = 5 \text{ V}, I_D = 20 \text{ A}, T_j = 250^\circ\text{C}$	80 50 43 35			

## B: Off State

Drain Leakage Current	$I_{DSS}$	$V_R = 600 \text{ V}, V_{GS} = 0 \text{ V}, T_j = 25^\circ\text{C}$ $V_R = 600 \text{ V}, V_{GS} = 0 \text{ V}, T_j = 175^\circ\text{C}$ $V_R = 600 \text{ V}, V_{GS} = 0 \text{ V}, T_j = 250^\circ\text{C}$	3 10 50		$\mu\text{A}$
Gate Leakage Current	$I_{SG}$	$V_{SG} = 20 \text{ V}, T_j = 25^\circ\text{C}$	20		nA

## C: Thermal

Thermal resistance, junction - case	$R_{ThJC}$	1.16	$^\circ\text{C/W}$
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## Section III: Dynamic Electrical Characteristics

Parameter	Symbol	Conditions	Values			Unit
			min.	typ.	max.	
<b>A: Capacitance and Gate Charge</b>						
Input Capacitance	$C_{iss}$	$V_{GS} = 0 \text{ V}, V_D = 100 \text{ V}, f = 1 \text{ MHz}$	2500			pF
Reverse Transfer/Output Capacitance	$C_{rss}/C_{oss}$	$V_D = 100 \text{ V}, f = 1 \text{ MHz}$	158			pF
Output Capacitance Stored Energy	$E_{oss}$	$V_{GS} = 0 \text{ V}, V_D = 100 \text{ V}, f = 1 \text{ MHz}$	0.8			$\mu\text{J}$
Effective Output Capacitance, time related	$C_{oss,tr}$	$I_D = \text{constant}, V_{GS} = 0 \text{ V}, V_{DS} = 0 \dots 100 \text{ V}$	260			pF
Effective Output Capacitance, energy related	$C_{oss,er}$	$V_{GS} = 0 \text{ V}, V_{DS} = 0 \dots 100 \text{ V}$	202			pF
Gate-Source Charge	$Q_{GS}$	$V_{GS} = -5 \dots 3 \text{ V}$	27			nC
Gate-Drain Charge	$Q_{GD}$	$V_{GS} = 0 \text{ V}, V_{DS} = 0 \dots 100 \text{ V}$	26			nC
Gate Charge - Total	$Q_G$		53			nC

 B: Switching<sup>1</sup>

Internal Gate Resistance – zero bias	$R_{G(INT-ZERO)}$	$f = 1 \text{ MHz}, V_{AC} = 50 \text{ mV}, V_{DS} = V_{GS} = 0 \text{ V}, T_j = 225^\circ\text{C}$	2.6		$\Omega$
Internal Gate Resistance – ON	$R_{G(INT-ON)}$	$V_{GS} > 2.5 \text{ V}, V_{DS} = 0 \text{ V}, T_j = 225^\circ\text{C}$	0.16		$\Omega$
Turn On Delay Time	$t_{d(on)}$	$T_j = 25^\circ\text{C}, V_{DS} = 400 \text{ V}, I_D = 20 \text{ A}, \text{Inductive Load}$	90		ns
Fall Time, $V_{DS}$	$t_f$		80		ns Fig. 11, 13
Turn Off Delay Time	$t_{d(off)}$	Refer to Section V: for additional driving information	50		ns
Rise Time, $V_{DS}$	$t_r$		55		ns Fig. 12, 14
Turn On Delay Time	$t_{d(on)}$	$T_j = 225^\circ\text{C}, V_{DS} = 400 \text{ V}, I_D = 20 \text{ A}, \text{Inductive Load}$	90		ns
Fall Time, $V_{DS}$	$t_f$		85		ns Fig. 11
Turn Off Delay Time	$t_{d(off)}$	Refer to Section V: for additional driving information	50		ns
Rise Time, $V_{DS}$	$t_r$		50		ns Fig. 12
Turn-On Energy Per Pulse	$E_{on}$	$T_j = 25^\circ\text{C}, V_{DS} = 400 \text{ V}, I_D = 20 \text{ A}, \text{Inductive Load}$	810		$\mu\text{J}$ Fig. 11, 13
Turn-Off Energy Per Pulse	$E_{off}$		95		$\mu\text{J}$ Fig. 12, 14
Total Switching Energy	$E_{tot}$		905		$\mu\text{J}$
Turn-On Energy Per Pulse	$E_{on}$	$T_j = 225^\circ\text{C}, V_{DS} = 400 \text{ V}, I_D = 20 \text{ A}, \text{Inductive Load}$	140		$\mu\text{J}$ Fig. 11
Turn-Off Energy Per Pulse	$E_{off}$		45		$\mu\text{J}$ Fig. 12
Total Switching Energy	$E_{tot}$		185		$\mu\text{J}$

<sup>1</sup> – All times are relative to the Drain-Source Voltage  $V_{DS}$

## Section IV: Figures

### A: Static Characteristics

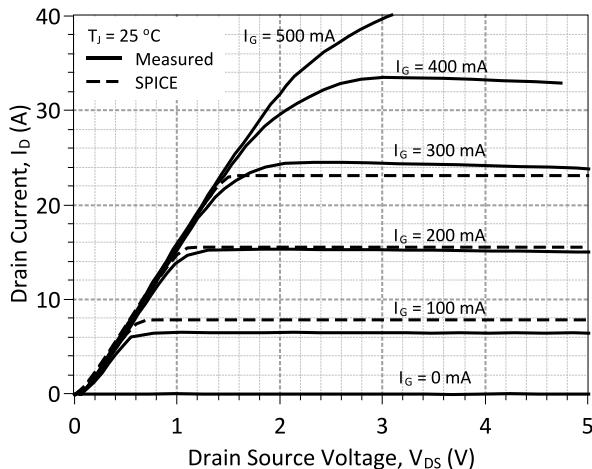


Figure 1: Typical Output Characteristics at 25 °C

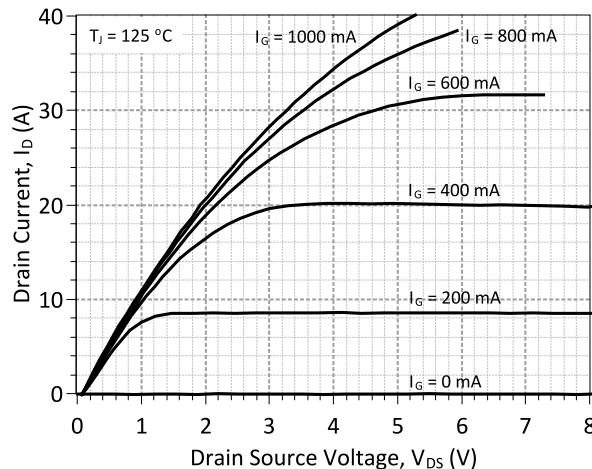


Figure 2: Typical Output Characteristics at 125 °C

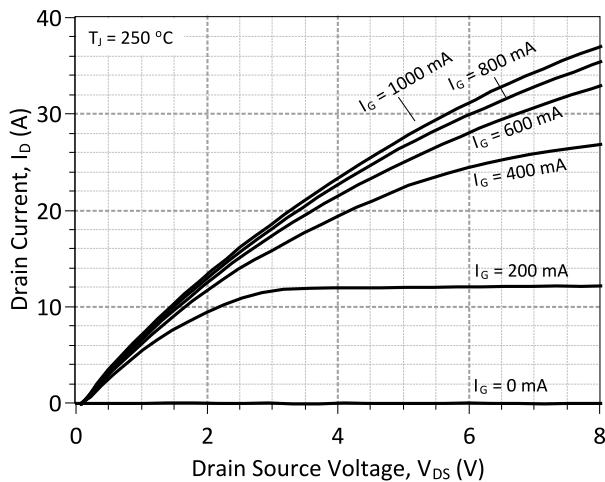


Figure 3: Typical Output Characteristics at 250 °C

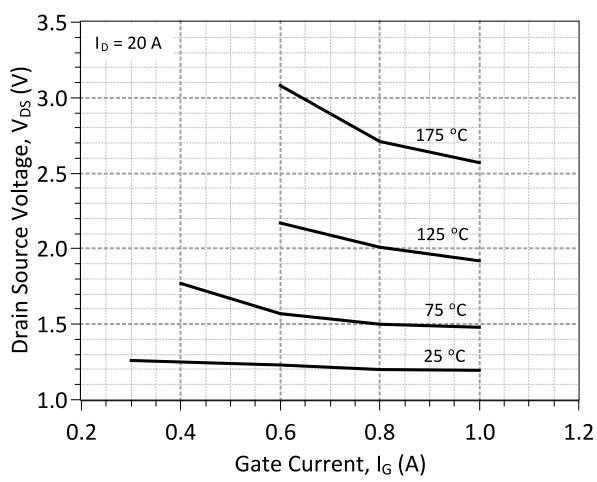


Figure 4: Drain-Source Voltage vs. Gate Current

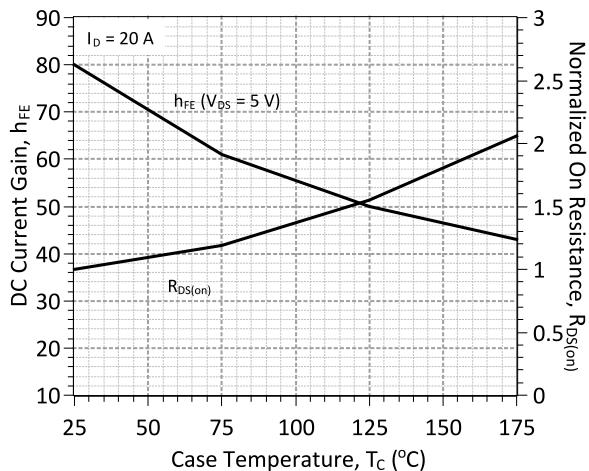


Figure 5: Normalized On-Resistance and Current Gain vs. Temperature

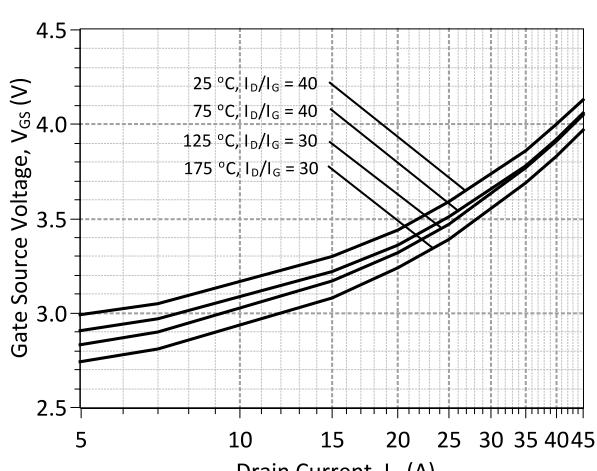
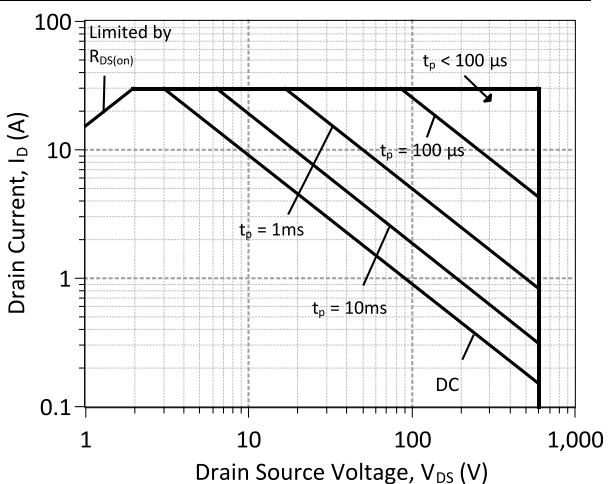
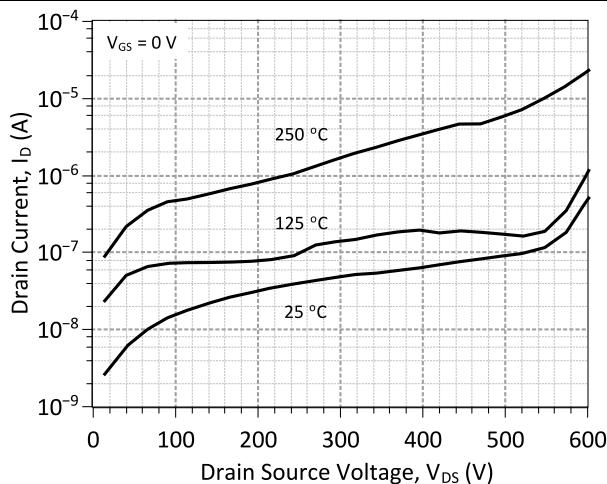
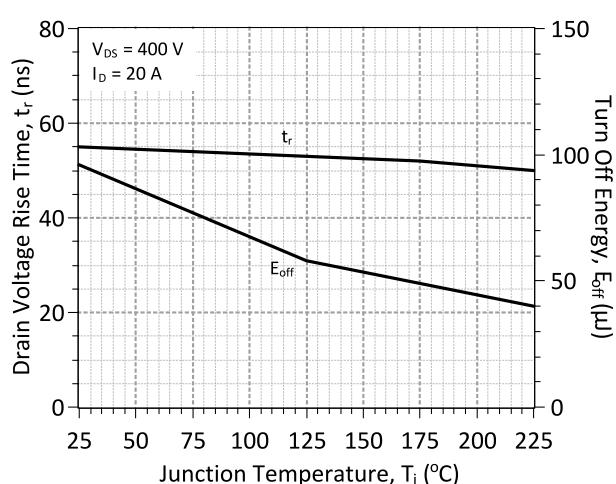
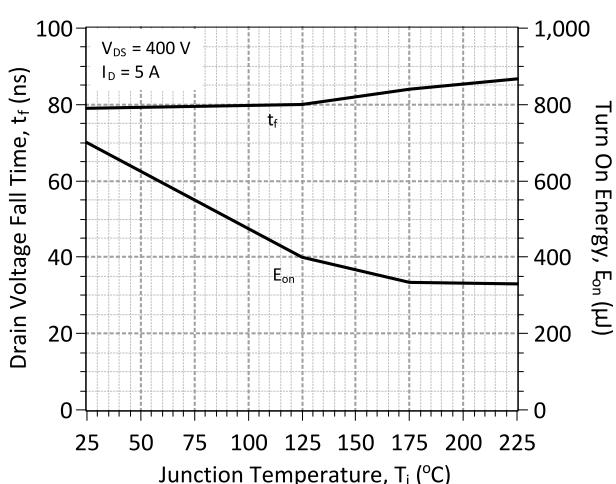
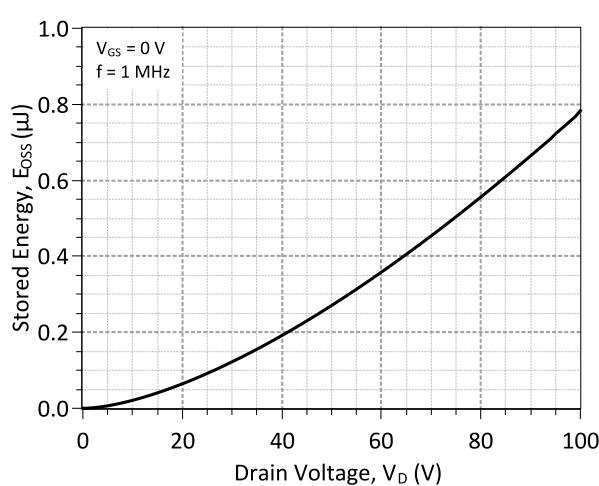
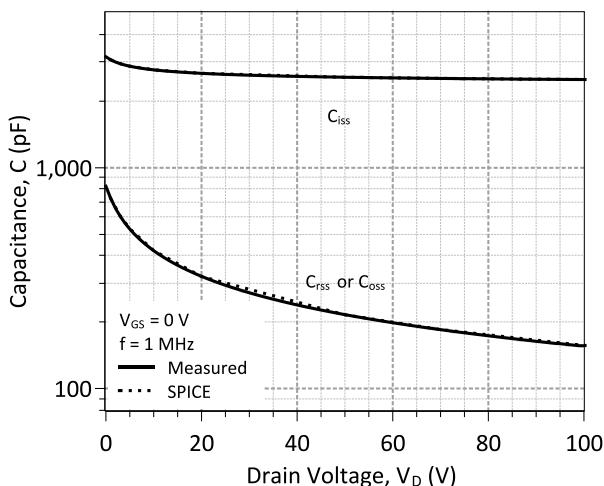
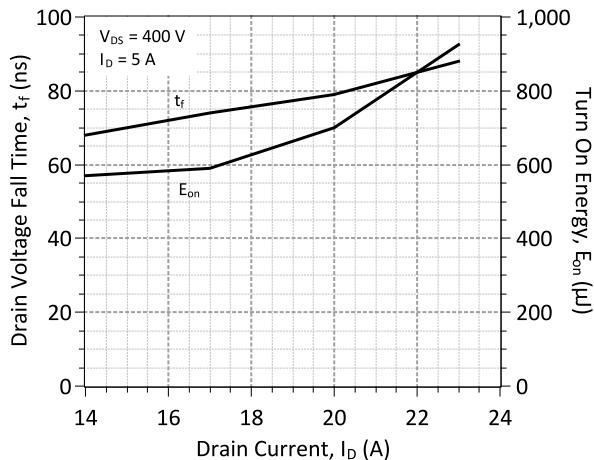


Figure 6: Typical Gate – Source Saturation Voltage

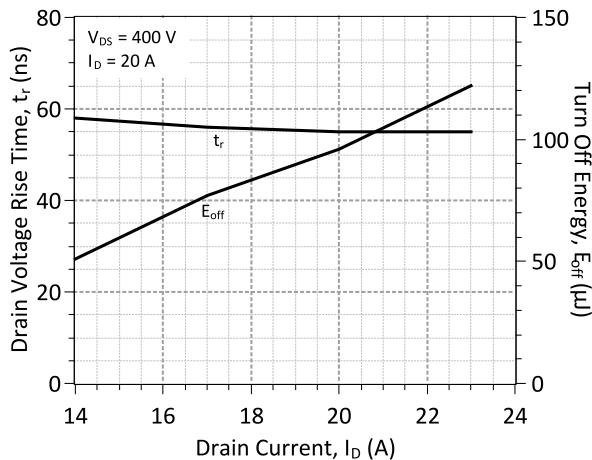


#### B: Dynamic Characteristics

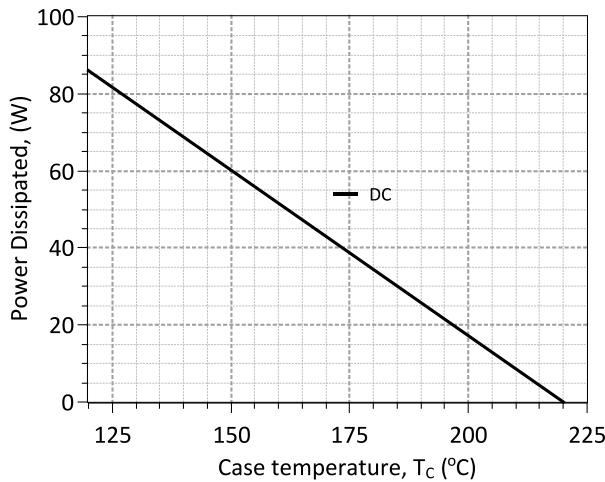




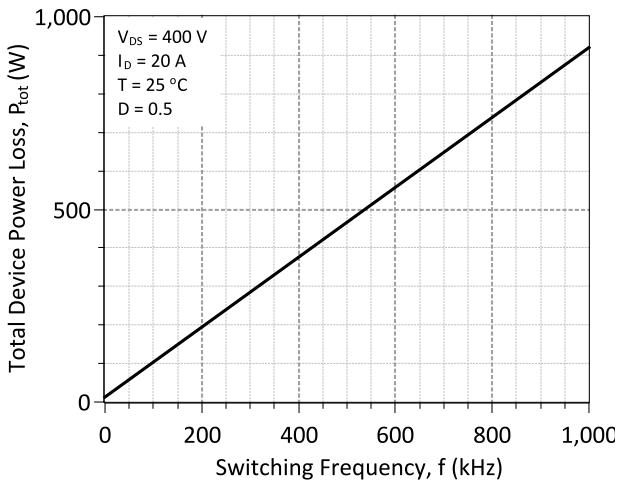
**Figure 13: Typical Turn On Energy Losses and Switching Times vs. Drain Current**



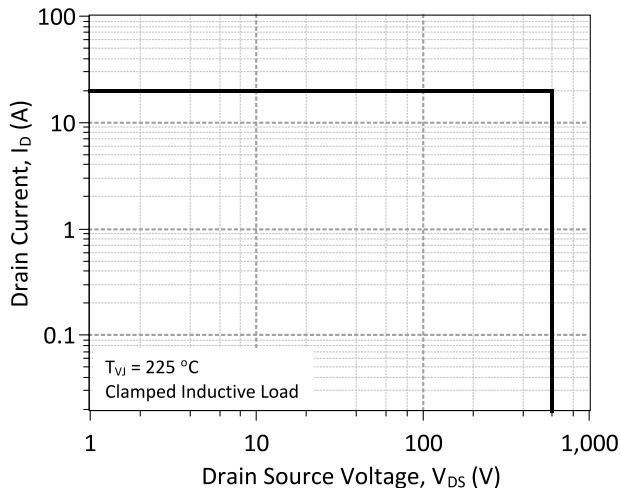
**Figure 14: Typical Turn Off Energy Losses and Switching Times vs. Drain Current**



**Figure 15: Power Derating Curve**

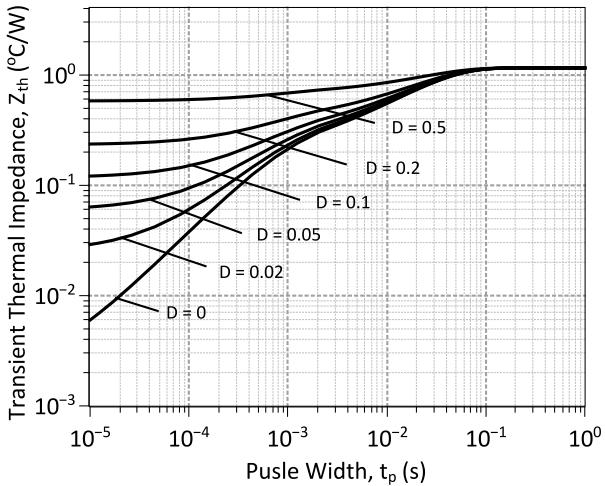


**Figure 16: Typical Hard Switched Device Power Loss vs. Switching Frequency<sup>2</sup>**



**Figure 17: Turn-Off Safe Operating Area**

<sup>2</sup> – Representative values based on device switching energy loss. Actual losses will depend on gate drive conditions, device load, and circuit topology.



**Figure 18: Transient Thermal Impedance**

## Section V: Driving the 2N7639-GA

The 2N7639-GA is a current controlled SiC transistor which requires a positive gate current for turn-on and to remain in on-state. It may be driven by different drive topologies depending on the intended application.

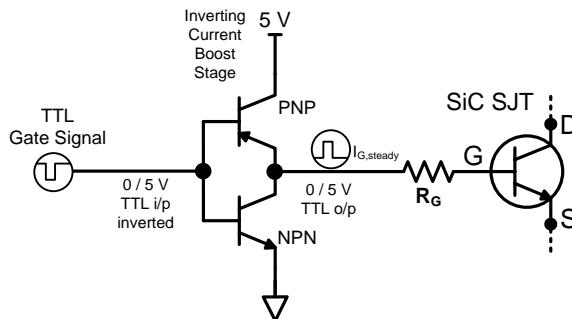
**Table 1: Estimated Power Consumption and switching frequencies for various Gate Drive topologies.**

Drive Topology	Gate Drive Power Consumption	Switching Frequency
Simple TTL	High	Low
Constant Current	Medium	Medium
High Speed – Boost Capacitor	Medium	High
High Speed – Boost Inductor	Low	High
Proportional	Lowest	Medium
Pulsed Power	Medium	N/A

### A: Simple TTL Drive

The 2N7639-GA may be driven by 5 V TTL logic by using a simple current amplification stage. The current amplifier output current must meet or exceed the steady state gate current,  $I_{G,steady}$ , required to operate the 2N7639-GA. An external gate resistor  $R_G$ , shown in the Figure 19 topology, sets  $I_{G,steady}$  to the required level which is dependent on the SJT drain current  $I_D$  and DC current gain  $h_{FE}$ .  $R_G$  may be calculated from the equation below. The values of  $h_{FE}$  and  $V_{GS,sat}$  may be read from Figure 5 and Figure 6, respectively.  $V_{EC,sat}$  can be taken from the PNP datasheet, a partial list of high-temperature PNP and NPN transistors options is given below. High-temperature MOSFETs may also be used in the topology.

$$R_{G,max} = \frac{(5.0 V - V_{EC,sat}(PNP) - V_{GS,sat}(SJT)) * h_{FE}(T, I_D)}{I_D * 1.5}$$



**Figure 19: Simple TTL Gate Drive Topology**

**Table 2: Partial List of High-Temperature BJTs for TTL Gate Driving**

BJT Part Number	Type	$T_{j,max}$ (°C)
PHPT60603PY	PNP	175
PHPT60603NY	NPN	175
2N2222	NPN	200
2N6730	PNP	200
2N2905	PNP	200
2N5883	PNP	200
2N5885	NPN	200

## B: High Speed Driving

For ultra high speed 2N7639-GA switching ( $t_r, t_f < 20$  ns) while maintaining low gate drive losses the supplied gate current should include a positive current peak during turn-on, a negative voltage peak during turn-off, and continuous gate current  $I_G$  to remain on.

An SJT is rapidly switched from its blocking state to on-state, when the necessary gate charge for turn-on,  $Q_G$ , is supplied by a burst of high gate current until the gate-source capacitance,  $C_{GS}$ , and gate-drain capacitance,  $C_{GD}$ , are fully charged. Ideally, the burst should terminate when the drain voltage has fallen to its on-state value in order to avoid unnecessary drive losses. A negative voltage peak is recommended for the turn-off transition in order to ensure that the gate current is not being supplied under high  $dV/dt$  due to the Miller effect. While satisfactory turn off can be achieved with  $V_{GS} = 0$  V, a negative  $V_{GS}$  value may be used in order to speed up the turn-off transition.

### B:1: High Speed, Low Loss Drive with Boost Capacitor

The 2N7639-GA may be driven using a High Speed, Low Loss Drive with Boost Capacitor topology in which multiple voltage levels, a gate resistor, and a gate capacitor are used to provide current peaks at turn-on and turn-off for fast switching and a continuous gate current while in on-state. As shown in Figure 20, in this topology two gate driver ICs are utilized. An external gate resistor  $R_G$  is driven by a low voltage driver to supply the continuous gate current throughout on-state and a gate capacitor  $C_G$  is driven at a higher voltage level to supply a high current peak at turn-on and turn-off. A 3 kV isolated evaluation gate drive board (GA03IDDJT30-FR4) from GeneSiC Semiconductor utilizing this topology is commercially available for high and low-side driving, its datasheet provides additional details about this drive topology.

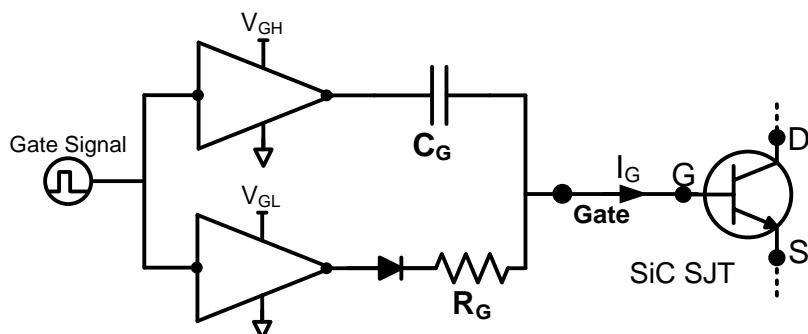


Figure 20: High Speed, Low Loss Drive with Boost Capacitor Topology

### B:2: High Speed, Low Loss Drive with Boost Inductor

A High Speed, Low-Loss Driver with Boost Inductor is also capable of driving the 2N7639-GA at high-speed. It utilizes a gate drive inductor instead of a capacitor to provide the high-current gate current pulses  $I_{G, on}$  and  $I_{G, off}$ . During operation, inductor  $L$  is charged to a specified  $I_{G, on}$  current value then made to discharge  $I_L$  into the SJT gate pin using logic control of  $S_1, S_2, S_3$ , and  $S_4$ , as shown in Figure 21. After turn on, while the device remains on the necessary steady state gate current  $I_{G, steady}$  is supplied from source  $V_{CC}$  through  $R_G$ . Please refer to the article "A current-source concept for fast and efficient driving of silicon carbide transistors" by Dr. Jacek Rabkowski for additional information on this driving topology.<sup>3</sup>

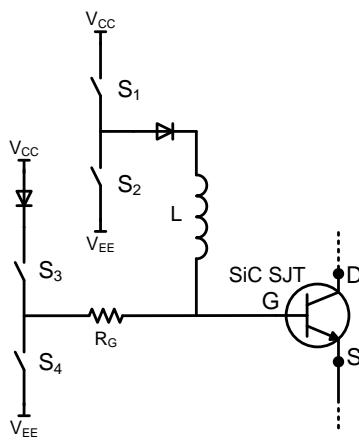


Figure 21: High Speed, Low-Loss Driver with Boost Inductor Topology

<sup>3</sup> – Archives of Electrical Engineering. Volume 62, Issue 2, Pages 333–343, ISSN (Print) 0004-0746, DOI: 10.2478/ae-2013-0026, June 2013

### C: Proportional Gate Current Driving

A proportional gate drive topology may be beneficial for applications in which the 2N7639-GA will operate over a wide range of drain current conditions to lower the gate drive power consumption. A proportional gate driver relies on instantaneous drain current  $I_D$  feedback to vary the steady state gate current  $I_{G,steady}$  supplied to the 2N7639-GA.

#### C:1: Voltage Controlled Proportional Driver

A voltage controlled proportional driver relies on a gate drive integrated circuit to detect the 2N7639-GA drain-source voltage  $V_{DS}$  during on-state to sense  $I_D$ . The integrated circuit will then increase or decrease  $I_G$  in response to  $I_D$ . This allows  $I_G$  and gate drive power consumption to reduce while  $I_D$  is low or for  $I_G$  to increase when  $I_D$  increases. A high voltage diode connected between the drain and sense protects the integrated circuit from high-voltage when blocking. A simplified version of this topology is shown in Figure 22. Additional information will be available in the future at <http://www.genesicsemi.com/references/product-notes/>.

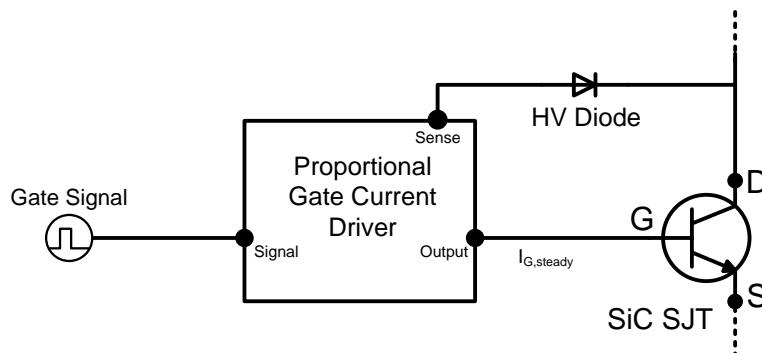


Figure 22: Simplified Voltage Controlled Proportional Driver

#### C:2: Current Controlled Proportional Driver

The current controlled proportional driver relies on a low-loss transformer in the drain or source path to provide feedback of the 2N7639-GA drain current during on-state to supply  $I_{G,steady}$  into the gate.  $I_{G,steady}$  will increase or decrease in response to  $I_D$  at a fixed forced current gain which is set by the turns ratio of the transformer,  $h_{force} = I_D / I_G = N_2 / N_1$ . 2N7639-GA is initially tuned-on using a gate current pulse supplied into an RC drive circuit to allow  $I_D$  current to begin flowing. This topology allows  $I_{G,steady}$  and the gate drive power consumption to reduce while  $I_D$  is relatively low or for  $I_{G,steady}$  to increase when  $I_D$  increases. A simplified version of this topology is shown in Figure 23. Additional information will be available in the future at <http://www.genesicsemi.com/references/product-notes/>.

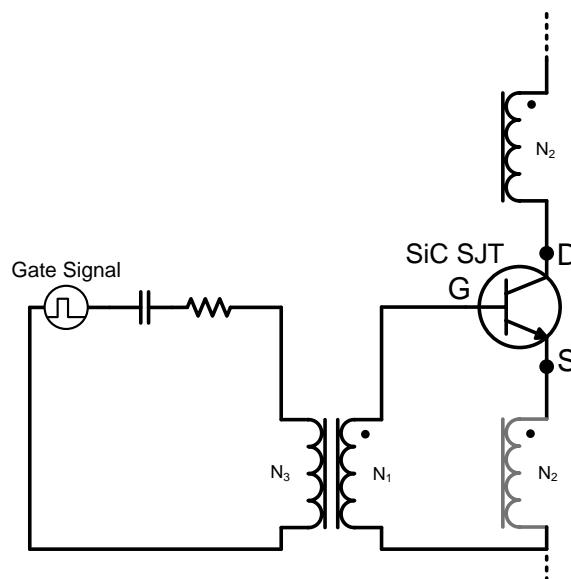
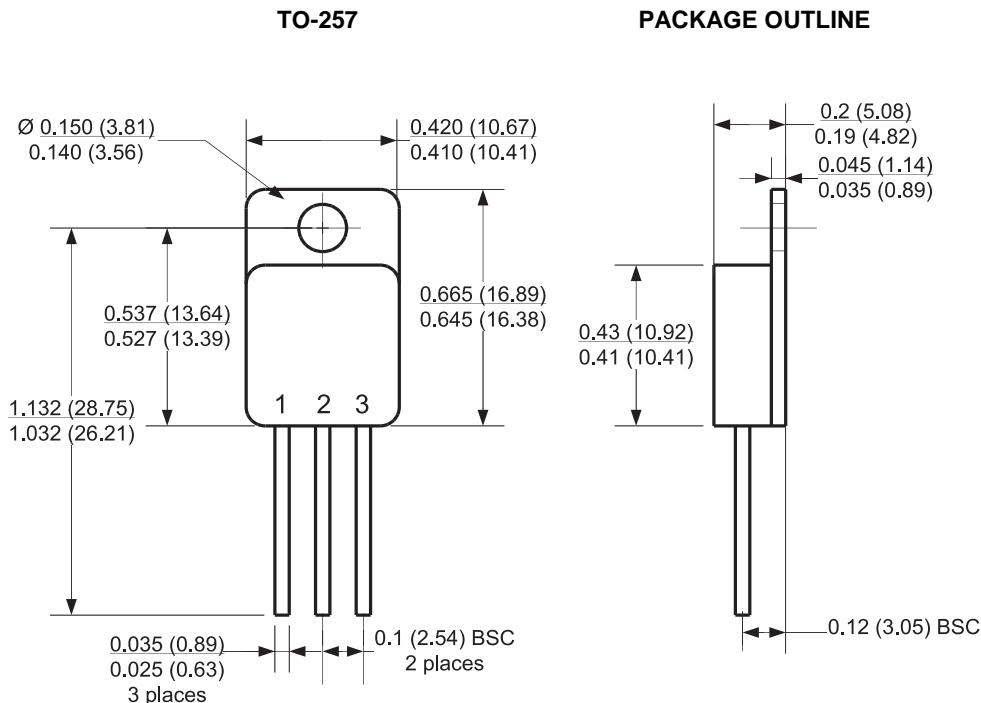


Figure 23: Simplified Current Controlled Proportional Driver

**Section VI: Package Dimensions**

**NOTE**

1. CONTROLLED DIMENSION IS INCH. DIMENSION IN BRACKET IS MILLIMETER.
2. DIMENSIONS DO NOT INCLUDE END FLASH, MOLD FLASH, MATERIAL PROTRUSIONS

Revision History				
Date	Revision	Comments	Supersedes	
2014/12/12	5	Updated Electrical Characteristics		
2014/08/25	4	Updated Electrical Characteristics		
2014/03/18	3	Updated Gate Drive Section		
2013/12/19	2	Updated Gate Drive Section		
2013/11/18	1	Updated Electrical Characteristics		
2012/08/24	0	Initial release		

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## Section VII: SPICE Model Parameters

This is a secure document. Please copy this code from the SPICE model PDF file on our website ([http://www.genesicsemi.com/images/hit\\_sic/sjt/2N7639-GA\\_SPICE.pdf](http://www.genesicsemi.com/images/hit_sic/sjt/2N7639-GA_SPICE.pdf)) into LTSPICE (version 4) software for simulation of the 2N7639-GA.

```
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*
*      $Revision: 1.3          $
*      $Date: 12-DEC-2014      $
*
*      GeneSiC Semiconductor Inc.
*      43670 Trade Center Place Ste. 155
*      Dulles, VA 20166
*
*      COPYRIGHT (C) 2014 GeneSiC Semiconductor Inc.
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*      OF ANY KIND EITHER EXPRESSED OR IMPLIED, INCLUDING BUT NOT LIMITED
*      TO ANY IMPLIED WARRANTIES OF MERCHANTABILITY AND FITNESS FOR A
*      PARTICULAR PURPOSE."
*      Models accurate up to 2 times rated drain current.
*
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+ ISE         1.0733E-26
+ EG          3.23
+ BF          110
+ BR          0.55
+ IKF         200
+ NF          1.02
+ NE          2.0
+ RB          2.6
+ IRB         0.002
+ RBM         0.16
+ RE          0.01
+ RC          0.045
+ CJC         8.2281E-10
+ VJC         3.31126
+ MJC         0.48117
+ CJE         2.33957E-9
+ VJE         2.91486
+ MJE         0.48211
+ XTI         3
+ XTB         -1.2
+ TRC1        6.20E-03
+ VCEO        600
+ ICRATING   32
+ MFG         GeneSiC_Semiconductor
*
* End of 2N7639-GA SPICE Model
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