

# Wide Supply Range, Rail-to-Rail Output Instrumentation Amplifier

**Data Sheet** 

### FEATURES

Gain set with 1 external resistor Gain range: 1 to 1000 Input voltage goes below ground Inputs protected beyond supplies Very wide power supply range Single supply: 2.2 V to 36 V Dual supplies: ±1.35 V to ±18 V Bandwidth (G = 1): 1.5 MHz CMRR (G = 1): 90 dB minimum for BR models Input noise: 22 nV/√Hz Typical supply current: 350 µA Specified temperature: -40°C to +125°C 8-lead SOIC and MSOP packages

### **APPLICATIONS**

Industrial process controls Bridge amplifiers Medical instrumentation Portable data acquisition Multichannel systems

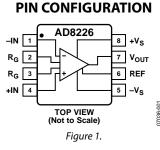
#### **GENERAL DESCRIPTION**

The AD8226 is a low cost, wide supply range instrumentation amplifier that requires only one external resistor to set any gain between 1 and 1000.

The AD8226 is designed to work with a variety of signal voltages. A wide input range and rail-to-rail output allow the signal to make full use of the supply rails. Because the input range also includes the ability to go below the negative supply, small signals near ground can be amplified without requiring dual supplies. The AD8226 operates on supplies ranging from  $\pm 1.35$  V to  $\pm 18$  V for dual supplies and 2.2 V to 36 V for single supply.

The robust AD8226 inputs are designed to connect to realworld sensors. In addition to its wide operating range, the

**AD8226** 



#### Table 1. Instrumentation Amplifiers by Category<sup>1</sup>

1 7 0 7							
General Purpose	Zero Drift	Military Grade	Low Power	High Speed PGA			
AD8220	AD8231	AD620	AD627	AD8250			
AD8221	AD8290	AD621	AD623	AD8251			
AD8222	AD8293	AD524	AD8223	AD8253			
AD8224	AD8553	AD526	AD8226				
AD8228	AD8556	AD624	AD8227				
AD8295	AD8557		AD8235/				
			AD8236				

<sup>1</sup> Visit www.analog.com for the latest instrumentation amplifiers.

AD8226 can handle voltages beyond the rails. For example, with a  $\pm 5$  V supply, the part is guaranteed to withstand  $\pm 35$  V at the input with no damage. Minimum as well as maximum input bias currents are specified to facilitate open wire detection.

The AD8226 is perfect for multichannel, space-constrained industrial applications. Unlike other low cost, low power instrumentation amplifiers, the AD8226 is designed with a minimum gain of 1 and can easily handle ±10 V signals. With its MSOP package and 125°C temperature rating, the AD8226 thrives in tightly packed, zero airflow designs.

The AD8226 is available in 8-lead MSOP and SOIC packages, and is fully specified for  $-40^{\circ}$ C to  $+125^{\circ}$ C operation.

For a device with a similar package and performance as the AD8226 but with gain settable from 5 to 1000, consider using the AD8227.

Rev. C

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### Comparable Parts

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### Evaluation Kits

• AD62x, AD822x, AD842x Series InAmp Evaluation Board

### Documentation 🖵

### **Data Sheet**

• AD8226: Wide Supply Range, Rail-to-Rail Output Instrumentation Amplifier Data Sheet

### **Technical Books**

• A Designer's Guide to Instrumentation Amplifiers, 3rd Edition, 2006

### **User Guides**

• UG-261: Evaluation Boards for the AD62x, AD822x and AD842x Series

### Tools and Simulations

- Inamp Common-Mode Range / Gain Calculator
- AD8226 SPICE Macro Model

### Reference Designs

- CN0213
- CN0251
- CN0253
- CN0289
- CN0295
- CN0325

### Reference Materials

### **Technical Articles**

- High-performance Adder Uses Instrumentation Amplifiers
- MS-2160: Mitigation Strategies for ECG Design Challenges
- MS-2178: Discussion Between CareFusion and Analog Devices: Optimizing Performance and Lowering Power in an EEG Amplifer

### Design Resources

- AD8226 Material Declaration
- PCN-PDN Information
- Quality And Reliability
- · Symbols and Footprints

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### **REVISION HISTORY**

### 9/12-Rev. B to Rev. C

Changes to CMRR, Voltage Offset, Input Offset Current, and	
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### 3/11-Rev. A to Rev. B

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### 7/09—Rev. 0 to Rev. A

Added BRZ and BRM Models Universal
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and Operating Range Parameter, Table 24
Changes to Common-Mode Rejection Ratio (CMRR) Parameter
and to Input Offset, $V_{OSO}$ , Average Temperature Coefficient
Parameter, Table 3
Changes to Gain vs. Temperature Parameter, Table 36
Changes to Gain Selection Section 19
Changes to Reference Terminal Section and Input Voltage
Range Section
Changes to Ordering Guide
1/09—Revision 0: Initial Version

# **SPECIFICATIONS**

 $+V_{s} = +15 \text{ V}, -V_{s} = -15 \text{ V}, V_{REF} = 0 \text{ V}, T_{A} = 25^{\circ}\text{C}, G = 1, R_{L} = 10 \text{ k}\Omega$ , specifications referred to input, unless otherwise noted.

### Table 2.

			ARZ, ARM	Z		BRZ, BRM	Z	
Parameter	Conditions	Min	Тур	Max	Min	Тур	Max	Unit
COMMON-MODE REJECTION RATIO (CMRR)	$V_{CM} = -10 \text{ V to } +10 \text{ V}$							
CMRR, DC to 60 Hz								
G = 1		86			90			dB
G = 10		106			106			dB
G = 100		120			120			dB
G = 1000		120			120			dB
CMRR at 5 kHz								
G = 1		80			80			dB
G = 10		90			90			dB
G = 100		90			90			dB
G = 1000		100			100			dB
NOISE	Total noise: $e_N = \sqrt{(e_{NI}^2 + (e_{NO}/G)^2)}$							
Voltage Noise	1 kHz							
Input Voltage Noise, e <sub>NI</sub>			22	24		22	24	nV/√Hz
Output Voltage Noise, e <sub>NO</sub>			120	125		120	125	nV/√Hz
RTI	f = 0.1 Hz to 10 Hz			. 20		.20	.20	,
G = 1			2			2		μV p-p
G = 10			0.5			0.5		μV p-p
G = 100 to 1000			0.4			0.4		μV p-p
Current Noise	f = 1  kHz		100			100		fA/√Hz
current tobe	f = 0.1  Hz to  10  Hz		3			3		pA p-p
VOLTAGE OFFSET	Total offset voltage:		5		-	J		hv h-h
VOLTAGE OFFSET	$V_{OS} = V_{OSI} + (V_{OSO}/G)$							
Input Offset, V <sub>OSI</sub>	$V_{s} = \pm 5 V \text{ to } \pm 15 V$			100			50	μV
Average Temperature Coefficient	$T_{A} = -40^{\circ}C \text{ to } +125^{\circ}C$		0.5	2		0.5	1	μV/°C
Output Offset, V <sub>oso</sub>	$V_s = \pm 5 \text{ V to } \pm 15 \text{ V}$			600			400	μV
Average Temperature Coefficient	$T_{A} = -40^{\circ}$ C to +125°C		2	10		1	5	μV/°C
Offset RTI vs. Supply (PSR)	$V_{s} = \pm 5 \text{ V to } \pm 15 \text{ V}$		-			•		p.,, c
G = 1	.,	100			100			dB
G = 10		115			115			dB
G = 100		120			120			dB
G = 1000		120			120			dB
INPUT CURRENT		120			120			40
Input Bias Current <sup>1</sup>	$T_A = +25^{\circ}C$	5	20	27	5	20	27	nA
•	$T_A = +125^{\circ}C$	5	15	25	5	15	25	nA
	$T_A = -40^{\circ}C$	5	30	35	5	30	35	nA
Average Temperature Coefficient	$T_{A} = -40^{\circ}C \text{ to } +125^{\circ}C$	-	70			70		pA/°C
Input Offset Current	$T_A = +25^{\circ}C$			1			0.5	nA
	$T_A = +125$ °C			1.5			0.5	nA
	$T_A = -40^{\circ}C$			2			0.5	nA
Average Temperature Coefficient	$T_{A} = -40^{\circ}$ C to +125°C		5	-		5	010	pA/°C
REFERENCE INPUT								10.4 0
R <sub>IN</sub>			100			100		kΩ
l <sub>in</sub>			7			7		μA
Voltage Range		-Vs		+Vs	$-V_s$		+Vs	V
Reference Gain to Output			1	د	2	1	د	V/V
Reference Gain Error			0.01			0.01		%
DYNAMIC RESPONSE	1	1						
Small-Signal –3 dB Bandwidth								
G = 1			1500			1500		kHz
G = 10			160			160		kHz
G = 100			20			20		kHz
G=1000			2			2		kHz

		A	ARZ, ARMZ			BRZ, BRMZ		
Parameter	Conditions	Min	Тур	Max	Min	Тур	Max	Unit
Settling Time 0.01%	10 V step							
G = 1			25			25		μs
G = 10			15			15		μs
G = 100			40			40		μs
G = 1000			350			350		μs
Slew Rate	G = 1		0.4			0.4		V/µs
	G = 5 to 100		0.6			0.6		V/µs
GAIN	$G = 1 + (49.4 \text{ k}\Omega/\text{R}_{G})$							
Gain Range		1		1000	1		1000	V/V
Gain Error	V <sub>OUT</sub> ±10 V							
G = 1				0.015			0.01	%
G = 5 to 1000				0.15			0.1	%
Gain Nonlinearity	$V_{OUT} = -10 V to +10 V$			0.15			0.1	/0
G = 1  to  10	$R_{\rm l} \ge 2  \mathrm{k}\Omega$			10			10	ppm
G = 100	$R_L \ge 2 k\Omega$ $R_L \ge 2 k\Omega$			75			75	ppm
G = 1000	$R_{\rm L} \ge 2 \ {\rm K}\Omega$ $R_{\rm I} \ge 2 \ {\rm k}\Omega$			750			750	
G = 1000 Gain vs. Temperature <sup>2</sup>	$N_L \ge 2 K \Omega 2$			750			750	ppm
G = 1	$T_A = -40^{\circ}C \text{ to } +85^{\circ}C$			F			1	
0=1				5 5			1	ppm
	$T_A = 85^{\circ}C \text{ to } 125^{\circ}C$						2	ppm
G > 1	$T_{A} = -40^{\circ}C \text{ to } +125^{\circ}C$			-100			-100	ppm
INPUT	$V_{s} = \pm 1.35 \text{ V to } +36 \text{ V}$							
Input Impedance								
Differential			0.8  2			0.8  2		GΩ
Common Mode			0.4  2			0.4  2		GΩ∥β
Input Operating Voltage Range <sup>3</sup>	$T_A = +25^{\circ}C$	$-V_{s} - 0.1$			$-V_{s} - 0.1$		$+V_{s}-0.8$	V
	$T_{A} = +125^{\circ}C$	$-V_{s} - 0.05$			$-V_{s} - 0.05$		$+V_{s}-0.6$	V
	$T_A = -40^{\circ}C$	$-V_{s} - 0.15$		$+V_{s}-0.9$	$-V_{s} - 0.15$		$+V_{s}-0.9$	V
Input Overvoltage Range	$T_{A} = -40^{\circ}C \text{ to } +125^{\circ}C$	$+V_{s} - 40$		$-V_{s} + 40$	$+V_{s} - 40$		$-V_{s} + 40$	V
OUTPUT								
Output Swing								
$R_L = 2 k\Omega$ to Ground								
	$T_A = +25^{\circ}C$	$-V_{s} + 0.4$		$+V_{s}-0.7$	$-V_{s} + 0.4$		$+V_{s}-0.7$	V
	$T_{A} = +125^{\circ}C$	$-V_{s} + 0.4$		+V <sub>s</sub> - 1.0	$-V_{s} + 0.4$		+V <sub>s</sub> - 1.0	V
	$T_A = -40^{\circ}C$	$-V_{s} + 1.2$		$+V_{s} - 1.1$	$-V_{s} + 1.2$		+V <sub>s</sub> - 1.1	V
$R_{I} = 10 k\Omega$ to Ground					-			
-	$T_A = +25^{\circ}C$	$-V_{s} + 0.2$		$+V_{s}-0.2$	$-V_{s} + 0.2$		$+V_{s}-0.2$	V
	$T_{A} = +125^{\circ}C$	$-V_{s} + 0.3$			$-V_{s} + 0.3$		$+V_{s} - 0.3$	V
	$T_A = -40^{\circ}C$	$-V_{s} + 0.2$			$-V_{s} + 0.2$		$+V_{s} - 0.2$	
$R_L = 100 \text{ k}\Omega$ to Ground		- 3			-3			
	$T_{A} = -40^{\circ}C \text{ to } +125^{\circ}C$	$-V_{s} + 0.1$		$+V_{s}-0.1$	$-V_{s} + 0.1$		$+V_{s} - 0.1$	v
Short-Circuit Current	T <sub>A</sub> = 40 C to 1125 C	V <sub>S</sub> I O.I	13	1 <b>v</b> <sub>S</sub> 0.1	<b>v</b> <sub>S</sub> i <b>0.1</b>	13	1 V <sub>S</sub> 0.1	mA
POWER SUPPLY			5			L J		
	Dual supply appration	±1 3E		<b>⊥</b> 10	±1.25		<b>±10</b>	v
Operating Range	Dual-supply operation	±1.35	250	±18	±1.35	250	±18	V
Quiescent Current	$T_A = +25^{\circ}C$		350	425		350	425	μA
	$T_A = -40^{\circ}C$		250	325		250	325	μA
	$T_A = +85^{\circ}C$		450	525		450	525	μA
	$T_{A} = +125^{\circ}C$		525	600		525	600	μA
TEMPERATURE RANGE		-40		+125	-40		+125	°C

<sup>1</sup> The input stage uses pnp transistors; therefore, input bias current always flows out of the part. <sup>2</sup> The values specified for G > 1 do not include the effects of the external gain-setting resistor, R<sub>c</sub>. <sup>3</sup> Input voltage range of the AD8226 input stage. The input range depends on the common-mode voltage, the differential voltage, the gain, and the reference voltage. See the Input Voltage Range section for more information.

# Data Sheet

 $+V_{s} = 2.7 V$ ,  $-V_{s} = 0 V$ ,  $V_{REF} = 0 V$ ,  $T_{A} = 25^{\circ}C$ , G = 1,  $R_{L} = 10 k\Omega$ , specifications referred to input, unless otherwise noted.

#### Table 3.

		ARZ, ARMZ			BRZ, BRMZ			
Parameter	Conditions	Min	Тур	Max	Min	Тур	Max	Unit
COMMON-MODE REJECTION RATIO (CMRR)	$V_{CM} = 0 V \text{ to } 1.7 V$							
CMRR, DC to 60 Hz								
G = 1		86			90			dB
G = 10		106			106			dB
G = 100		120			120			dB
G = 1000		120			120			dB
CMRR at 5 kHz								
G = 1		80			80			dB
G = 10		90			90			dB
G = 100		90			90			dB
G = 1000		100			100			dB
NOISE	Total noise: $e_N = \sqrt{(e_{NI}^2 + (e_{NO}/G)^2)}$							
Voltage Noise	1 kHz							
Input Voltage Noise, e <sub>NI</sub>			22	24		22	24	nV/√Hz
Output Voltage Noise, e <sub>NO</sub>			120	125		120	125	nV/√Hz
RTI	f = 0.1 Hz to 10 Hz		120	125		120	125	1107 9112
G = 1			2.0			2.0		μV p-p
G = 1 G = 10			0.5			0.5		μV p-p μV p-p
G = 100 G = 100 to 1000			0.5			0.5		μν p-p μV p-p
Current Noise	f = 1 kHz		0.4 100			0.4 100		μv ρ-ρ fA/√Hz
Current Noise	f = 0.1 Hz to 10 Hz		3			3		
VOLTAGE OFFSET			3			3		рА р-р
	Total offset voltage: $V_{OS} = V_{OSI} + (V_{OSO}/G)$			100			50	/
Input Offset, V <sub>OSI</sub>	T 40%C to 125%C		0.5	100		0.5	50	μV
Average Temperature Coefficient	$T_A = -40^{\circ}C \text{ to } +125^{\circ}C$		0.5	2		0.5	1	μV/°C
Output Offset, V <sub>oso</sub>	T 40%C to 125%C		2	600		1	400	μV
Average Temperature Coefficient	$T_A = -40^{\circ}C \text{ to } +125^{\circ}C$		2	10		1	5	μV/°C
Offset RTI vs. Supply (PSR)	$V_{s} = 0 V \text{ to } 1.7 V$	100			100			10
G = 1		100			100			dB
G = 10		115			115			dB
G = 100		120			120			dB
G = 1000		120			120			dB
INPUT CURRENT		_			_			
Input Bias Current <sup>1</sup>	$T_A = +25^{\circ}C$	5	20	27	5	20	27	nA
	$T_A = +125^{\circ}C$	5	15	25	5	15	25	nA
	$T_A = -40^{\circ}C$	5	30	35	5	30	35	nA
Average Temperature Coefficient	$T_{A} = -40^{\circ}C \text{ to } +125^{\circ}C$		70			70		pA/°C
Input Offset Current	$T_A = +25^{\circ}C$			1			0.5	nA
	$T_{A} = +125^{\circ}C$			1.5			0.5	nA
	$T_A = -40^{\circ}C$			1			0.1	nA
Average Temperature Coefficient	$T_{A} = -40^{\circ}C \text{ to } +125^{\circ}C$		5			5		pA/°C
REFERENCE INPUT								
R <sub>IN</sub>			100			100		kΩ
I <sub>IN</sub>			7			7		μΑ
Voltage Range		$-V_{s}$		$+V_s$	$-V_s$		+Vs	V
Reference Gain to Output			1			1		V/V
Reference Gain Error			0.01			0.01		%
DYNAMIC RESPONSE								
Small-Signal –3 dB Bandwidth								
G = 1			1500			1500		kHz
G = 10			160			160		kHz
G = 100			20			20		kHz
G = 1000			2			2		kHz

		A	ARZ, ARN	٨Z	BRZ, BRMZ			
Parameter	Conditions	Min	Тур	Max	Min	Тур	Max	Unit
Settling Time 0.01%	2 V step							
G = 1			6			6		μs
G = 10			6			6		μs
G = 100			35			35		μs
G = 1000			350			350		μs
Slew Rate	G = 1		0.4			0.4		V/µs
	G = 5 to 100		0.6			0.6		V/µs
GAIN	$G = 1 + (49.4 \text{ k}\Omega/\text{R}_{G})$							
Gain Range		1		1000	1		1000	V/V
Gain Error								
G = 1	$V_{OUT} = 0.8 V \text{ to } 1.8 V$			0.04			0.01%	%
G = 5 to 1000	$V_{OUT} = 0.2 \text{ V to } 2.5 \text{ V}$			0.3			0.1%	%
Gain vs. Temperature <sup>2</sup>								
G = 1	$T_A = -40^{\circ}C$ to $+85^{\circ}C$			5			1	ppm/°
	$T_{A} = +85^{\circ}C \text{ to } +125^{\circ}C$			5			2	ppm/°
G > 1	$T_{A} = -40^{\circ}C \text{ to } +125^{\circ}C$			-100			-100	ppm/°
INPUT	$-V_s = 0 V_r + V_s = 2.7 V \text{ to } 36 V$							
Input Impedance								
Differential			0.8  2			0.8  2		GΩ  pF
Common Mode			0.4  2			0.4  2		GΩ  pF
Input Operating Voltage Range <sup>3</sup>	$T_A = +25^{\circ}C$	-0.1		$+V_{s} - 0.7$	-0.1		$+V_{s}-0.7$	v
	$T_A = -40^{\circ}C$	-0.15		$+V_{5} - 0.9$	-0.15		$+V_{s} - 0.9$	V
	$T_{A} = +125^{\circ}C$	-0.05		$+V_{5} - 0.6$	-0.05		$+V_{s} - 0.6$	V
Input Overvoltage Range	$T_{A} = -40^{\circ}C \text{ to } +125^{\circ}C$	$+V_{s} - 40$		$-V_{s} + 40$	$+V_{s} - 40$		$-V_{s} + 40$	
OUTPUT								
Output Swing	$R_L = 10 k\Omega$ to 1.35 V, $T_A = -40^{\circ}$ C to +125°C	0.1		$+V_{s}-0.1$	0.1		$+V_{s}-0.1$	v
Short-Circuit Current			13			13		mA
POWER SUPPLY		1						1
Operating Range	Single-supply operation	2.2		36	2.2		36	v
Quiescent Current	$T_A = +25^{\circ}C_{,} -V_S = 0 V_{,} +V_S = 2.7 V_{,}$		325	400		325	400	μA
	$T_A = -40^{\circ}C, -V_S = 0 V, +V_S = 2.7 V$		250	325		250	325	μA
	$T_A = +85^{\circ}C, -V_S = 0 V, +V_S = 2.7 V$		425	500		425	500	μA
	$T_A = +125^{\circ}C, -V_S = 0 V, +V_S = 2.7 V$		475	550		475	550	μA
TEMPERATURE RANGE		-40		+125	-40		+125	°C

<sup>1</sup> Input stage uses pnp transistors; therefore, input bias current always flows out of the part.
 <sup>2</sup> The values specified for G > 1 do not include the effects of the external gain-setting resistor, R<sub>c</sub>.
 <sup>3</sup> Input voltage range of the AD8226 input stage. The input range depends on the common-mode voltage, the differential voltage, the gain, and the reference voltage. See the Input Voltage Range section for more information.

# **ABSOLUTE MAXIMUM RATINGS**

#### Table 4.

Parameter	Rating
Supply Voltage	±18 V
Output Short-Circuit Current	Indefinite
Maximum Voltage at –IN or +IN	$-V_{s} + 40 V$
Minimum Voltage at –IN or +IN	$+V_{s} - 40 V$
REF Voltage	±Vs
Storage Temperature Range	–65°C to +150°C
Specified Temperature Range	-40°C to +125°C
Maximum Junction Temperature	140°C
ESD	
Human Body Model	1.5 kV
Charge Device Model	1.5 kV
Machine Model	100 V

Stresses above those listed under Absolute Maximum Ratings may cause permanent damage to the device. This is a stress rating only; functional operation of the device at these or any other conditions above those indicated in the operational section of this specification is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

### THERMAL RESISTANCE

 $\theta_{\text{IA}}$  is specified for a device in free air.

#### Table 5. Thermal Resistance

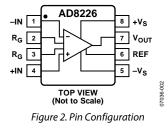
Package	θ <sub>JA</sub>	Unit
8-Lead MSOP, 4-Layer JEDEC Board	135	°C/W
8-Lead SOIC, 4-Layer JEDEC Board	121	°C/W

### **ESD CAUTION**



**ESD** (electrostatic discharge) sensitive device. Charged devices and circuit boards can discharge without detection. Although this product features patented or proprietary protection circuitry, damage may occur on devices subjected to high energy ESD. Therefore, proper ESD precautions should be taken to avoid performance degradation or loss of functionality.

# **PIN CONFIGURATION AND FUNCTION DESCRIPTIONS**



#### Table 6. Pin Function Descriptions

Pin No.	Mnemonic	Description
1	-IN	Negative Input.
2, 3	R <sub>G</sub>	Gain-Setting Pins. Place a gain resistor between these two pins.
4	+IN	Positive Input.
5	$-V_s$	Negative Supply.
6	REF	Reference. This pin must be driven by low impedance.
7	V <sub>OUT</sub>	Output.
8	+V <sub>s</sub>	Positive Supply.

# **TYPICAL PERFORMANCE CHARACTERISTICS**

T = 25°C, V<sub>s</sub> = ±15 V, R<sub>L</sub> = 10 kΩ, unless otherwise noted.

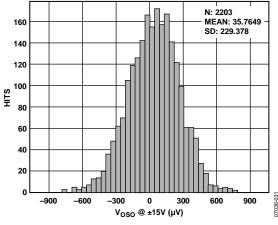


Figure 3. Typical Distribution of Output Offset Voltage

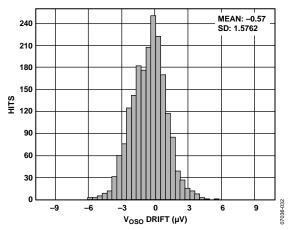


Figure 4. Typical Distribution of Output Offset Voltage Drift

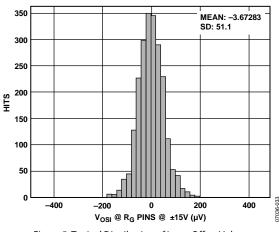


Figure 5. Typical Distribution of Input Offset Voltage

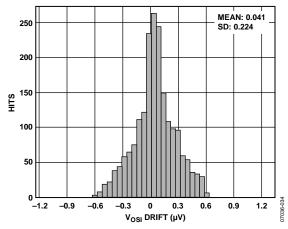


Figure 6. Typical Distribution of Input Offset Voltage Drift, G = 100

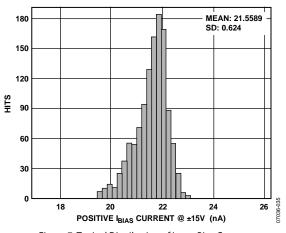


Figure 7. Typical Distribution of Input Bias Current

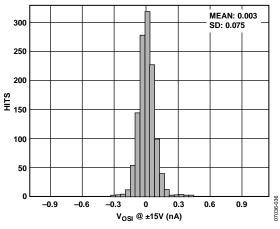
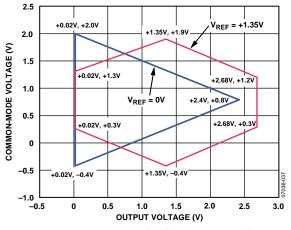
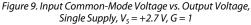
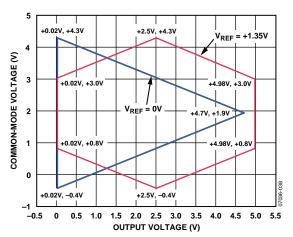
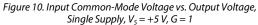


Figure 8. Typical Distribution of Input Offset Current









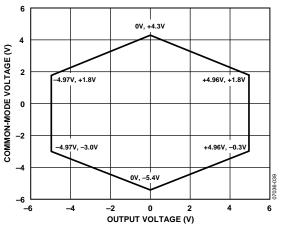


Figure 11. Input Common-Mode Voltage vs. Output Voltage, Dual Supplies,  $V_S = \pm 5$  V, G = 1

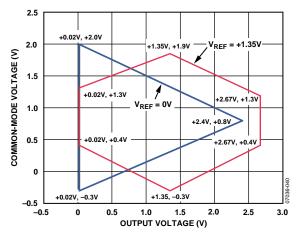


Figure 12. Input Common-Mode Voltage vs. Output Voltage, Single Supply,  $V_s = +2.7 V$ , G = 100

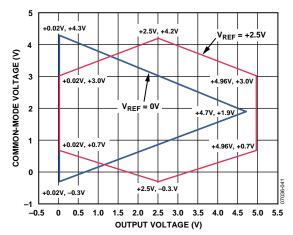


Figure 13. Input Common-Mode Voltage vs. Output Voltage, Single Supply,  $V_s = +5 V$ , G = 100

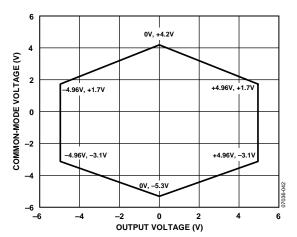


Figure 14. Input Common-Mode Voltage vs. Output Voltage, Dual Supplies,  $V_{S} = \pm 5 V$ , G = 100

### **Data Sheet**

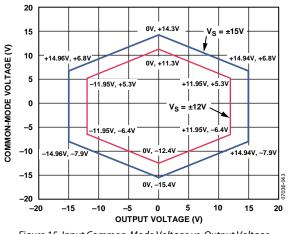
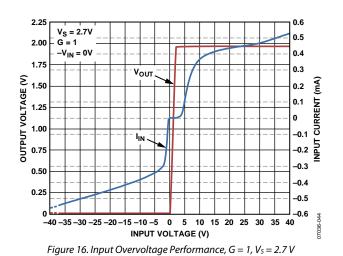


Figure 15. Input Common-Mode Voltage vs. Output Voltage, Dual Supplies,  $V_S = \pm 15 V$ , G = 1



0.5 16  $V_S = \pm 15V$ 14 G = 1 0.4 12  $-V_{IN} = 0V$ 10 0.3 VOUT 8 OUTPUT VOLTAGE (V) 6 0.2 CURRENT (mA) 4 0.1 2 IIN 0 0 -2 -0.1 INPUT ( -4 -6 -0.2 -8 -0.3 -10 -12 -0.4 -14 -16 -0.5 7036-045 40 -35 -30 -25 -20 -15 -10 -5 0 5 10 15 20 25 30 35 40 INPUT VOLTAGE (V) Figure 17. Input Overvoltage Performance, G = 1,  $V_S = \pm 15 V$ 

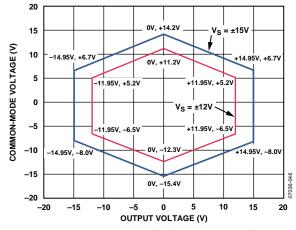
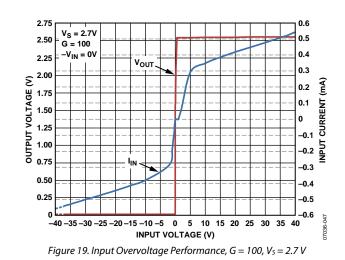
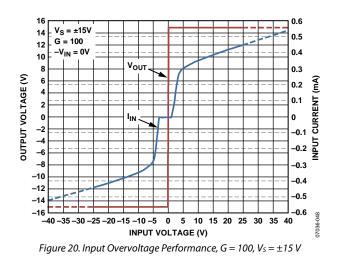


Figure 18. Input Common-Mode Voltage vs. Output Voltage, Dual Supplies,  $V_S = \pm 15 V$ , G = 100





**Data Sheet** 

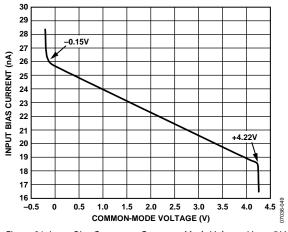


Figure 21. Input Bias Current vs. Common-Mode Voltage,  $V_s = +5 V$ 

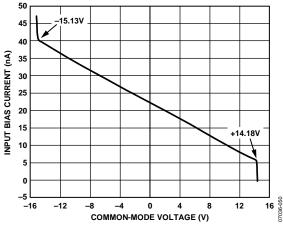


Figure 22. Input Bias Current vs. Common-Mode Voltage,  $V_{\rm S} = \pm 15$  V

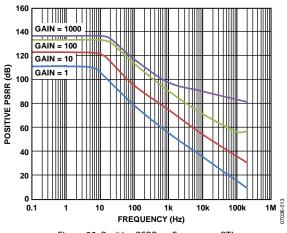
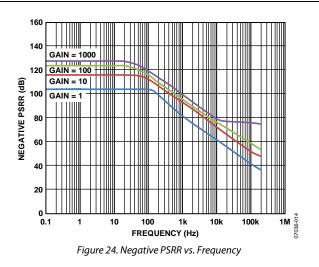
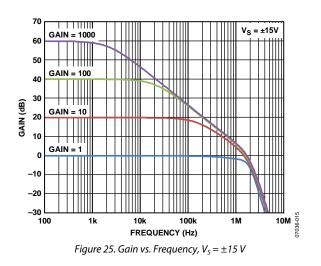


Figure 23. Positive PSRR vs. Frequency, RTI





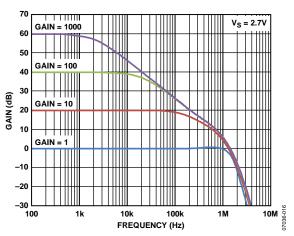
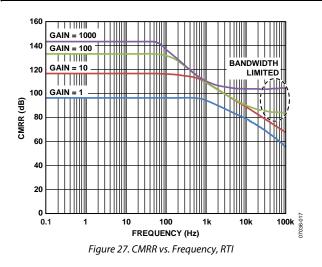
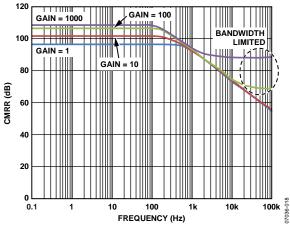
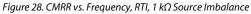


Figure 26. Gain vs. Frequency, 2.7 V Single Supply

### **Data Sheet**







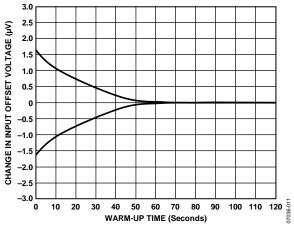


Figure 29. Change in Input Offset Voltage vs. Warm-Up Time

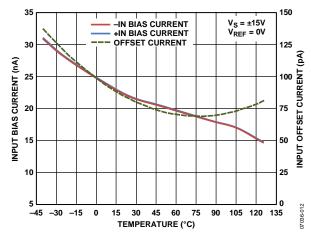
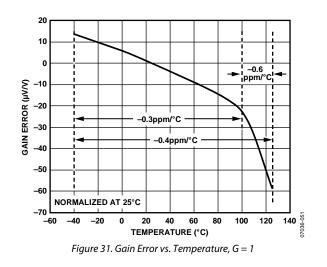
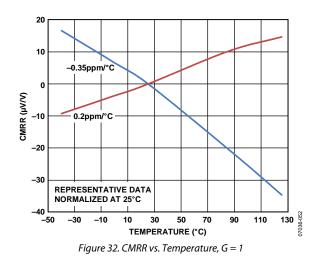
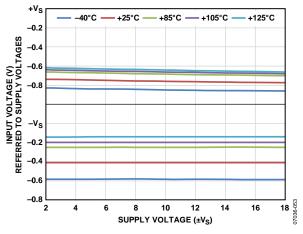
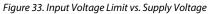


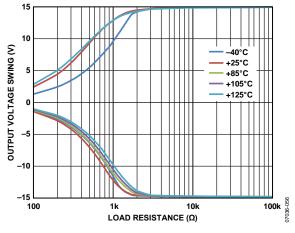
Figure 30. Input Bias Current and Input Offset Current vs. Temperature

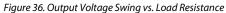












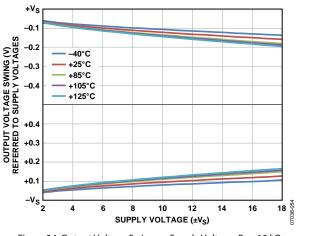


Figure 34. Output Voltage Swing vs. Supply Voltage,  $R_L = 10 k\Omega$ 

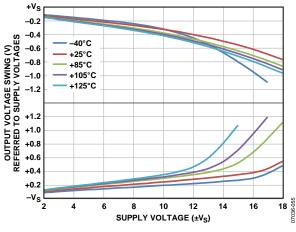


Figure 35. Output Voltage Swing vs. Supply Voltage,  $R_L = 2 k\Omega$ 

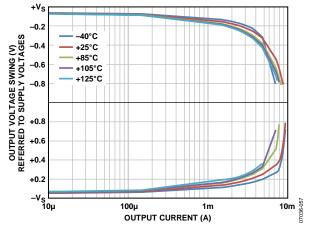
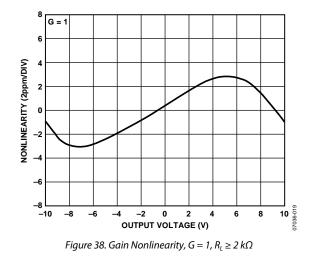
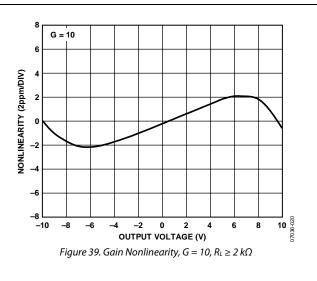
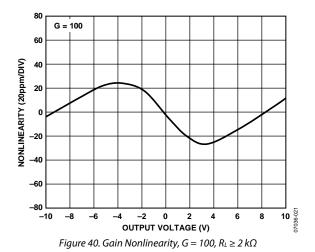


Figure 37. Output Voltage Swing vs. Output Current, G = 1



# Data Sheet





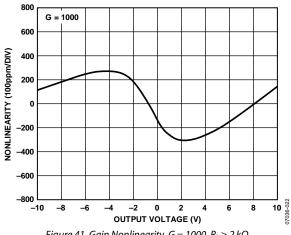
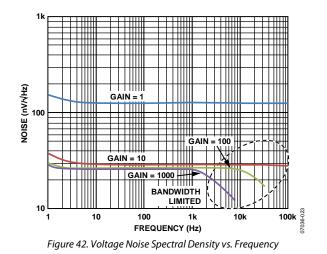


Figure 41. Gain Nonlinearity, G = 1000,  $R_L \ge 2 k\Omega$ 



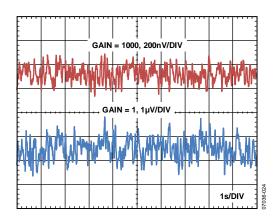
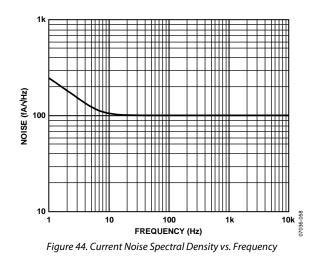


Figure 43. 0.1 Hz to 10 Hz RTI Voltage Noise, G = 1, G = 1000



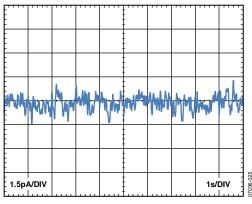


Figure 45. 0.1 Hz to 10 Hz Current Noise

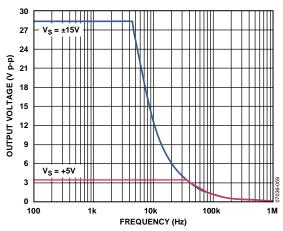
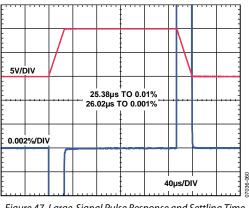
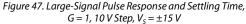


Figure 46. Large-Signal Frequency Response





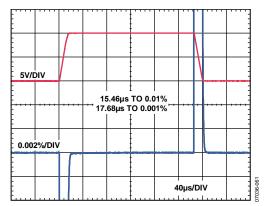


Figure 48. Large-Signal Pulse Response and Settling Time, G = 10, 10 V Step,  $V_{\rm S}$  =  $\pm 15$  V

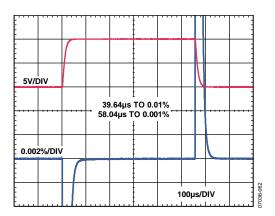


Figure 49. Large-Signal Pulse Response and Settling Time, G = 100, 10 V Step,  $V_{\rm S} = \pm 15 V$ 

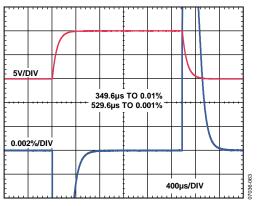


Figure 50. Large-Signal Pulse Response and Settling Time, G = 1000, 10 V Step,  $V_{\rm S} = \pm 15 V$ 

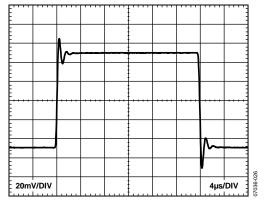


Figure 51. Small-Signal Response, G = 1,  $R_L = 10 k\Omega$ ,  $C_L = 100 pF$ 

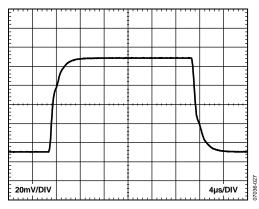


Figure 52. Small-Signal Response, G = 10,  $R_L = 10 \text{ k}\Omega$ ,  $C_L = 100 \text{ pF}$ 

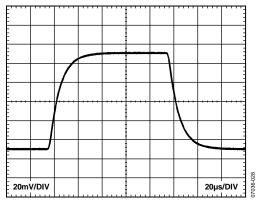


Figure 53. Small-Signal Response, G = 100,  $R_L = 10 \text{ k}\Omega$ ,  $C_L = 100 \text{ pF}$ 

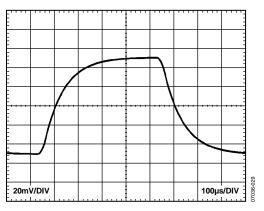


Figure 54. Small-Signal Response, G = 1000,  $R_L = 10 \text{ k}\Omega$ ,  $C_L = 100 \text{ pF}$ 

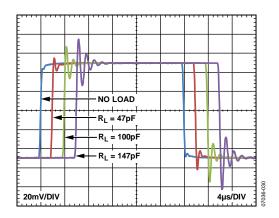


Figure 55. Small-Signal Response with Various Capacitive Loads,  $G=1, R_L=\infty$ 

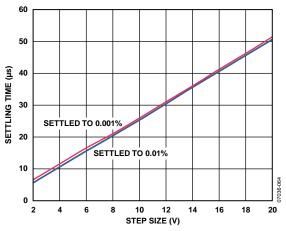


Figure 56. Settling Time vs. Step Size,  $V_s = \pm 15$  V Dual Supplies

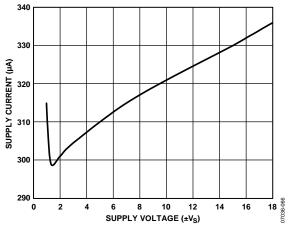


Figure 57. Supply Current vs. Supply Voltage

# THEORY OF OPERATION

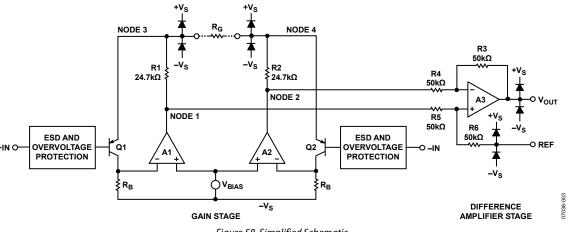


Figure 58. Simplified Schematic

### ARCHITECTURE

The AD8226 is based on the classic 3-op-amp topology. This topology has two stages: a preamplifier to provide differential amplification, followed by a difference amplifier to remove the common-mode voltage. Figure 58 shows a simplified schematic of the AD8226.

The first stage works as follows: in order to maintain a constant voltage across the bias resistor  $R_B$ , A1 must keep Node 3 a constant diode drop above the positive input voltage. Similarly, A2 keeps Node 4 at a constant diode drop above the negative input voltage. Therefore, a replica of the differential input voltage is placed across the gain-setting resistor,  $R_G$ . The current that flows across this resistance must also flow through the R1 and R2 resistors, creating a gained differential signal between the A2 and A1 outputs. Note that, in addition to a gained differential signal, the original common-mode signal, shifted a diode drop up, is also still present.

The second stage is a difference amplifier, composed of A3 and four 50 k $\Omega$  resistors. The purpose of this stage is to remove the common-mode signal from the amplified differential signal.

The transfer function of the AD8226 is

$$V_{OUT} = G(V_{IN+} - V_{IN-}) + V_{REF}$$

where:

$$G = 1 + \frac{49.4 \text{ k}\Omega}{R_G}$$

### **GAIN SELECTION**

Placing a resistor across the  $R_G$  terminals sets the gain of the AD8226, which can be calculated by referring to Table 7 or by using the following gain equation:

$$R_G = \frac{49.4 \text{ k}\Omega}{G - 1}$$

#### Table 7. Gains Achieved Using 1% Resistors

1% Standard Table Value of $R_G(\Omega)$	Calculated Gain
49.9 k	1.990
12.4 k	4.984
5.49 k	9.998
2.61 k	19.93
1.00 k	50.40
499	100.0
249	199.4
100	495.0
49.9	991.0

The AD8226 defaults to G = 1 when no gain resistor is used. The tolerance and gain drift of the  $R_G$  resistor should be added to the AD8226 specifications to determine the total gain accuracy of the system. When the gain resistor is not used, gain error and gain drift are minimal.

If a gain of 5 is required and minimal gain drift is important, consider using the AD8227. The AD8227 has a default gain of 5 that is set with internal resistors. Because all resistors are internal, the gain drift is extremely low (<5 ppm/°C maximum).

### **REFERENCE TERMINAL**

The output voltage of the AD8226 is developed with respect to the potential on the reference terminal. This is useful when the output signal needs to be offset to a precise midsupply level. For example, a voltage source can be tied to the REF pin to levelshift the output so that the AD8226 can drive a single-supply ADC. The REF pin is protected with ESD diodes and should not exceed either  $+V_s$  or  $-V_s$  by more than 0.3 V.

For the best performance, source impedance to the REF terminal should be kept below 2  $\Omega$ . As shown in Figure 58, the reference terminal, REF, is at one end of a 50 k $\Omega$  resistor. Additional impedance at the REF terminal adds to this 50 k $\Omega$  resistor and results in amplification of the signal connected to the positive input. The amplification from the additional R<sub>REF</sub> can be computed by 2(50 k $\Omega$  + R<sub>REF</sub>)/(100 k $\Omega$  + R<sub>REF</sub>).

Only the positive signal path is amplified; the negative path is unaffected. This uneven amplification degrades CMRR.

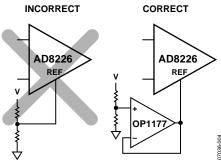


Figure 59. Driving the Reference Pin

### **INPUT VOLTAGE RANGE**

Figure 9 through Figure 15 and Figure 18 show the allowable common-mode input voltage ranges for various output voltages and supply voltages. The 3-op-amp architecture of the AD8226 applies gain in the first stage before removing common-mode voltage with the difference amplifier stage. Internal nodes between the first and second stages (Node 1 and Node 2 in Figure 58) experience a combination of a gained signal, a common-mode signal, and a diode drop. This combined signal can be limited by the voltage supplies even when the individual input and output signals are not limited.

For most applications, Figure 9 through Figure 15 and Figure 18 provide sufficient information to achieve a good design. For applications where a more detailed understanding is needed, Equation 1 to Equation 3 can be used to understand how the gain (G), common-mode input voltage ( $V_{CM}$ ), differential input voltage ( $V_{DIFF}$ ), and reference voltage ( $V_{REF}$ ) interact. The values for the constants,  $V_{-LIMIT}$ ,  $V_{+LIMIT}$ , and  $V_{REF\_LIMIT}$ , are shown in Table 8. These three formulas, along with the input and output range specifications in Table 2 and Table 3, set the operating boundaries of the part.

$$V_{CM} - \left| \frac{(V_{DIFF})(G)}{2} \right| > -V_{s} + V_{-LIMIT}$$
(1)

$$V_{CM} + \left| \frac{(V_{DIFF})(G)}{2} \right| < +V_S - V_{+LIMIT}$$
<sup>(2)</sup>

$$\frac{(V_{DIFF})(G)}{2} + V_{CM} + V_{REF}}_{2} < +V_{S} - V_{REF\_LIMIT}$$
(3)

Table 8. Input Voltage Range Constants for Various	
Temperatures	

Temperature	V_LIMIT	$V_{+\text{LIMIT}}$	
-40°C	-0.55 V	0.8 V	1.3 V
+25°C	-0.35 V	0.7 V	1.15 V
+85°C	-0.15 V	0.65 V	1.05 V
+125°C	-0.05 V	0.6 V	0.9 V

### Performance Across Temperature

The common-mode input range shifts upward with temperature. At cold temperatures, the part requires extra headroom from the positive supply, and operation near the negative supply has more margin. Conversely, hot temperatures require less headroom from the positive supply, but are the worst-case conditions for input voltages near the negative supply.

#### **Recommendation for Best Performance**

A typical part functions up to the boundaries described in this section. However, for best performance, designing with a few hundred millivolts extra margin is recommended. As signals approach the boundary, internal transistors begin to saturate, which can affect frequency and linearity performance.

If the application requirements exceed the boundaries, one solution is to apply less gain with the AD8226, and then apply additional gain later in the signal chain. Another option is to use the pin-compatible AD8227.

### LAYOUT

To ensure optimum performance of the AD8226 at the PCB level, care must be taken in the design of the board layout. The AD8226 pins are arranged in a logical manner to aid in this task.

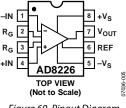


Figure 60. Pinout Diagram

### Common-Mode Rejection Ratio Over Frequency

Poor layout can cause some of the common-mode signals to be converted to differential signals before reaching the in-amp. Such conversions occur when one input path has a frequency response that is different from the other. To keep CMRR across frequency high, the input source impedance and capacitance of each path should be closely matched. Additional source resistance in the input path (for example, for input protection) should be placed close to the in-amp inputs, which minimizes their interaction with parasitic capacitance from the PCB traces.

Parasitic capacitance at the gain-setting pins can also affect CMRR over frequency. If the board design has a component at the gain-setting pins (for example, a switch or jumper), the part should be chosen so that the parasitic capacitance is as small as possible.

#### **Power Supplies**

A stable dc voltage should be used to power the instrumentation amplifier. Note that noise on the supply pins can adversely affect performance. For more information, see the PSRR performance curves in Figure 23 and Figure 24.

A 0.1  $\mu$ F capacitor should be placed as close as possible to each supply pin. As shown in Figure 61, a 10  $\mu$ F tantalum capacitor can be used farther away from the part. In most cases, it can be shared by other precision integrated circuits.

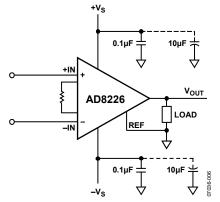


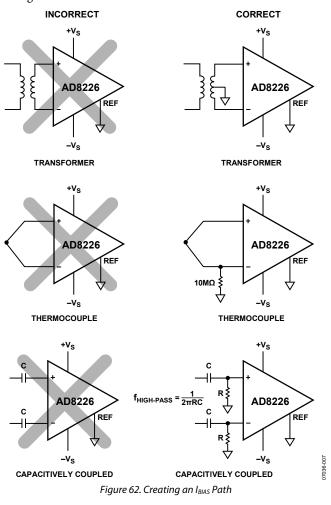
Figure 61. Supply Decoupling, REF, and Output Referred to Local Ground

#### References

The output voltage of the AD8226 is developed with respect to the potential on the reference terminal. Care should be taken to tie REF to the appropriate local ground.

### **INPUT BIAS CURRENT RETURN PATH**

The input bias current of the AD8226 must have a return path to ground. When the source, such as a thermocouple, cannot provide a return current path, one should be created, as shown in Figure 62.



### INPUT PROTECTION

The AD8226 has very robust inputs and typically does not need additional input protection. Input voltages can be up to 40 V from the opposite supply rail. For example, with a +5 V positive supply and a -8 V negative supply, the part can safely withstand voltages from -35 V to 32 V. Unlike some other instrumentation amplifiers, the part can handle large differential input voltages even when the part is in high gain. Figure 16, Figure 17, Figure 19, and Figure 20 show the behavior of the part under overvoltage conditions.

The rest of the AD8226 terminals should be kept within the supplies. All terminals of the AD8226 are protected against ESD.

For applications where the AD8226 encounters voltages beyond the allowed limits, external current-limiting resistors and lowleakage diode clamps such as the BAV199L, the FJH1100s, or the SP720 should be used.

### **RADIO FREQUENCY INTERFERENCE (RFI)**

RF rectification is often a problem when amplifiers are used in applications having strong RF signals. The disturbance can appear as a small dc offset voltage. High frequency signals can be filtered with a low-pass RC network placed at the input of the instrumentation amplifier, as shown in Figure 63. The filter limits the input signal bandwidth according to the following relationship:

$$FilterFrequency_{DIFF} = \frac{1}{2\pi R(2C_D + C_C)}$$
$$FilterFrequency_{CM} = \frac{1}{2\pi RC_C}$$

where  $C_D \ge 10 \text{ C}_{\text{C}}$ .

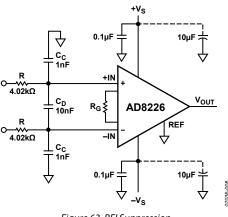


Figure 63. RFI Suppression

 $C_D$  affects the difference signal and  $C_C$  affects the common-mode signal. Values of R and  $C_C$  should be chosen to minimize RFI. Mismatch between the  $R \times C_C$  at the positive input and the  $R \times C_C$ at the negative input degrades the CMRR of the AD8226. By using a value of  $C_D$  that is one magnitude larger than  $C_C$ , the effect of the mismatch is reduced and performance is improved.

### APPLICATIONS INFORMATION DIFFERENTIAL DRIVE

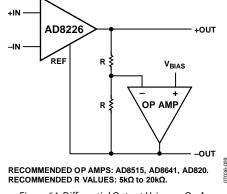


Figure 64. Differential Output Using an Op Amp

Figure 64 shows how to configure the AD8226 for differential output.

The differential output is set by the following equation:

 $V_{DIFF_OUT} = V_{OUT+} - V_{OUT-} = Gain \times (V_{IN+} - V_{IN-})$ 

The common-mode output is set by the following equation:

 $V_{CM_{OUT}} = (V_{OUT+} - V_{OUT-})/2 = V_{BIAS}$ 

The advantage of this circuit is that the dc differential accuracy depends on the AD8226, not on the op amp or the resistors. In addition, this circuit takes advantage of the precise control that the AD8226 has of its output voltage relative to the reference voltage. Although the dc performance and resistor matching of the op amp affect the dc common-mode output accuracy, such errors are likely to be rejected by the next device in the signal chain and therefore typically have little effect on overall system accuracy.

### **Tips for Best Differential Output Performance**

For best ac performance, an op amp with at least a 2 MHz gain bandwidth and a 1 V/ $\mu$ s slew rate is recommended. Good choices for op amps are the AD8641, AD8515, and AD820.

Keep trace lengths from the resistors to the inverting terminal of the op amp as short as possible. Excessive capacitance at this node can cause the circuit to be unstable. If capacitance cannot be avoided, use lower value resistors.

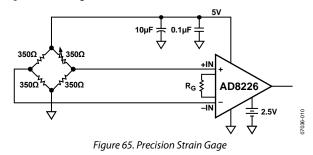
For best linearity and ac performance, a minimum positive supply voltage (+V<sub>s</sub>) is required. Table 9 shows the minimum supply voltage required for optimum performance. In this mode,  $V_{\rm CM\_MAX}$  indicates the maximum common-mode voltage expected at the input of the AD8226.

Table 9. Minimum Positive Supply Voltage

Temperature	Equation
Less than -10°C	$+V_{s} > (V_{CM_{MAX}} + V_{BIAS})/2 + 1.4 V$
–10°C to 25°C	$+V_{s} > (V_{CM_{MAX}} + V_{BIAS})/2 + 1.25 V$
More than 25°C	$+V_{S} > (V_{CM_{MAX}} + V_{BIAS})/2 + 1.1 V$

### PRECISION STRAIN GAGE

The low offset and high CMRR over frequency of the AD8226 make it an excellent candidate for performing bridge measurements. The bridge can be connected directly to the inputs of the amplifier (see Figure 65).



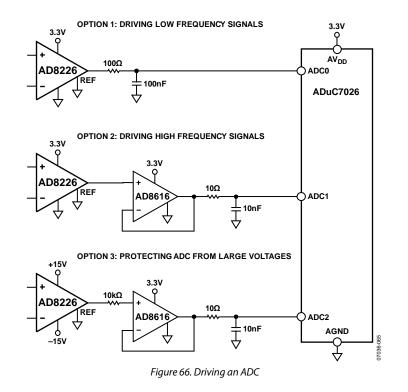
### **DRIVING AN ADC**

Figure 66 shows several methods for driving an ADC. The ADuC7026 microcontroller was chosen for this example because it contains ADCs with an unbuffered, charge-sampling architecture that is typical of most modern ADCs. This type of architecture typically requires an RC buffer stage between the ADC and amplifier to work correctly.

Option 1 shows the minimum configuration required to drive a charge-sampling ADC. The capacitor provides charge to the ADC sampling capacitor while the resistor shields the AD8226 from the capacitance. To keep the AD8226 stable, the RC time constant of the resistor and capacitor needs to stay above 5  $\mu$ s. This circuit is mainly useful for lower frequency signals.

Option 2 shows a circuit for driving higher speed signals. It uses a precision op amp (AD8616) with relatively high bandwidth and output drive. This amplifier can drive a resistor and capacitor with a much higher time constant and is therefore suited for higher frequency applications.

Option 3 is useful for applications where the AD8226 needs to run off a large voltage supply but drive a single-supply ADC. In normal operation, the AD8226 output stays within the ADC range, and the AD8616 simply buffers it. However, in a fault condition, the output of the AD8226 may go outside the supply range of both the AD8616 and the ADC. This is not an issue in the circuit, however, because the 10 k $\Omega$  resistor between the two amplifiers limits the current into the AD8616 to a safe level.



## **OUTLINE DIMENSIONS**

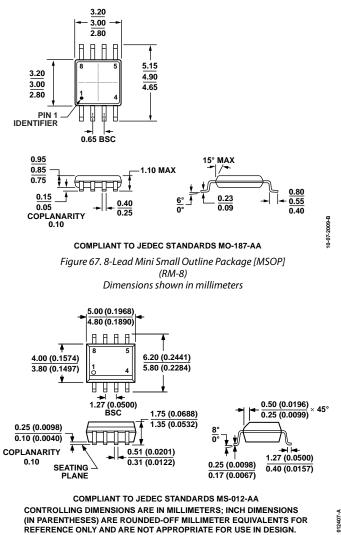


Figure 68. 8-Lead Standard Small Outline Package [SOIC\_N] Narrow Body (R-8)

#### Dimensions shown in millimeters and (inches)

#### **ORDERING GUIDE**

Model <sup>1</sup>	Temperature Range	Package Description	Package Option	Branding
AD8226ARMZ	-40°C to +125°C	8-Lead MSOP	RM-8	Y18
AD8226ARMZ-RL	-40°C to +125°C	8-Lead MSOP, 13" Tape and Reel	RM-8	Y18
AD8226ARMZ-R7	-40°C to +125°C	8-Lead MSOP, 7" Tape and Reel	RM-8	Y18
AD8226ARZ	-40°C to +125°C	8-Lead SOIC_N	R-8	
AD8226ARZ-RL	-40°C to +125°C	8-Lead SOIC_N, 13" Tape and Reel	R-8	
AD8226ARZ-R7	-40°C to +125°C	8-Lead SOIC_N, 7" Tape and Reel	R-8	
AD8226BRMZ	-40°C to +125°C	8-Lead MSOP	RM-8	Y19
AD8226BRMZ-RL	-40°C to +125°C	8-Lead MSOP, 13" Tape and Reel	RM-8	Y19
AD8226BRMZ-R7	-40°C to +125°C	8-Lead MSOP, 7" Tape and Reel	RM-8	Y19
AD8226BRZ	-40°C to +125°C	8-Lead SOIC_N	R-8	
AD8226BRZ-RL	-40°C to +125°C	8-Lead SOIC_N, 13" Tape and Reel	R-8	
AD8226BRZ-R7	-40°C to +125°C	8-Lead SOIC_N, 7" Tape and Reel	R-8	

<sup>1</sup> Z = RoHS Compliant Part.

# NOTES

# NOTES

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