



MPQ2169

6V, Dual 1.4A/1.4A or 2A/0.8A
Low Quiescent Current,
Synchronous Buck with PG and SS
AEC-Q100 Qualified

DESCRIPTION

The MPQ2169 is an internally compensated, dual, PWM, synchronous, step-down regulator that operates from a 2.7V to 6V input and generates an output voltage as low as 0.6V. The MPQ2169 can be configured as a 1.4A/1.4A or 2A/0.8A output current regulator and is ideal for powering portable equipment that runs on a single-cell lithium-ion (Li+) battery due to its low 60 μ A quiescent current.

The MPQ2169 integrates dual, 60m Ω , high-side switches and 25m Ω synchronous rectifiers to achieve high efficiency without an external Schottky diode. The MPQ2169 has peak-current-mode control and internal compensation and is capable of low dropout configurations. Both channels can operate at 100% duty cycle.

Full protection features include cycle-by-cycle current limit and thermal shutdown.

The MPQ2169 requires a minimal number of readily available, standard, external components and is available in QFN-18 (2mmx3mm) and QFN-18 (2.5mmx3.5mm) packages.

FEATURES

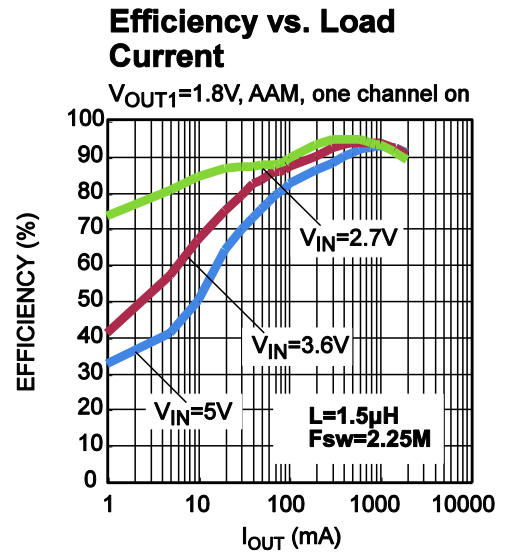
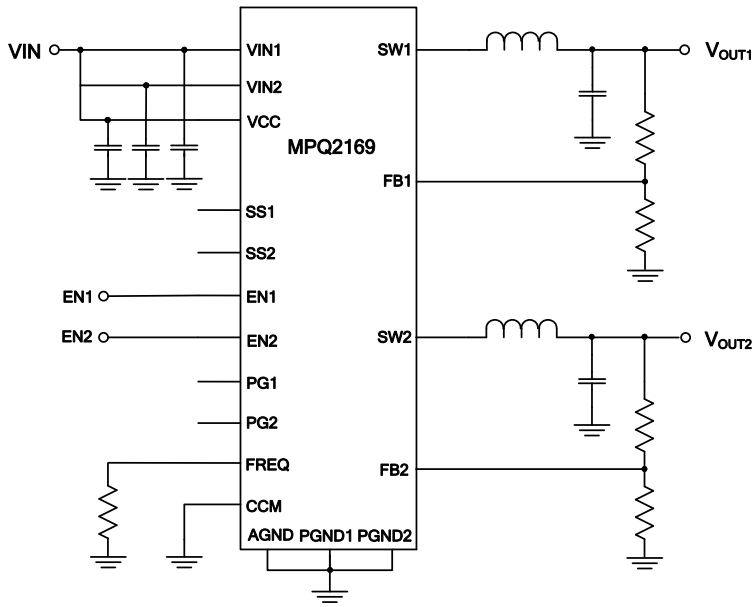
- 2.7V to 6V Operating Input Range
- 1.4A/1.4A or 2A/0.8A Continuous Current
- 60m Ω /25m Ω R_{DS(ON)}
- Programmed Frequency up to 3MHz
- External Sync Clock up to 3MHz
- 180° Phase-Shifted Operation
- Power Good (PG) Indicators
- External Soft Start (SS) and Track
- Adjustable Advanced Asynchronous Mode (AAM) or Forced Continuous Conduction Mode (FCCM)
- Peak Efficiency >90%
- Output Adjustable from 0.6V to 5.5V
- 100% Duty Cycle Operation
- 60 μ A Quiescent Current
- Cycle-by-Cycle Over-Current Protection (OCP)
- Short-Circuit Protection (SCP) with Hiccup Mode and Valley Current Detection
- Thermal Shutdown
- Available in QFN-18 (2mmx3mm) and QFN-18 (2.5mmx3.5mm) Packages
- Available in a Wettable Flank Package
- Available in AEC-Q100 Grade-1

APPLICATIONS

- Infotainment
- Cluster
- Telematics
- Battery-Power Devices
- Portable Instruments

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TYPICAL APPLICATION



ORDERING INFORMATION

Part Number*	Package	Top Marking
MPQ2169GDE-AEC1**	QFN-18 (2mmx3mm)	See Below
MPQ2169GRHE-AEC1**	QFN-18 (2.5mmx3.5mm)	See Below

* For Tape & Reel, add suffix -Z (e.g.: MPQ2169GRHE-Z).

** Wettable Flank

TOP MARKING (MPQ2169GDE-AEC1)

BJL
YWW
LLL

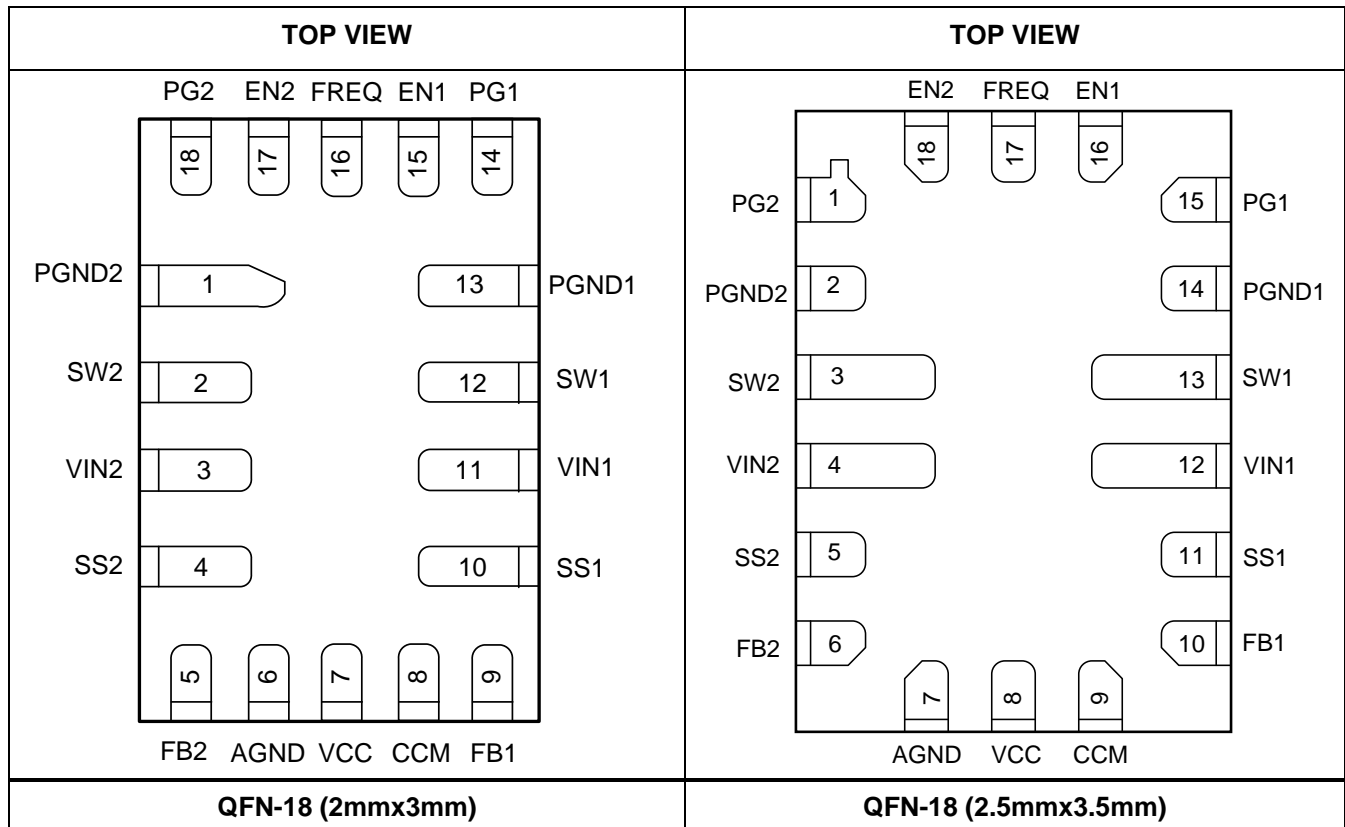
TOP MARKING (MPQ2169GRHE-AEC1)

AZZ
YWW
LLL

BJL: Product code of MPQ2169GDE-AEC1
Y: Year code
WW: Week code
LLL: Lot number

AZZ: Product code of MPQ2169GRHE-AEC1
Y: Year code
WW: Week code
LLL: Lot number

PACKAGE REFERENCE



PIN FUNCTIONS

QFN-18 (2x3) Pin #	QFN-18 (2.5x3.5) Pin #	Name	Description
1	2	PGND2	Power ground for channel 2. Connect PGND2 with larger copper areas to the negative terminals of the input and output capacitors. PGND2 must be connected to PGND1 on board externally.
2	3	SW2	Switch node connection to the inductor for channel 2. SW2 connects to the internal high- and low-side power MOSFET switches of the channel 2 buck.
3	4	VIN2	Input supply for channel 2. Place a decoupling capacitor to ground close to VIN2 to reduce switching spikes.
4	5	SS2	Soft start for channel 2.
5	6	FB2	Feedback for channel 2. FB2 is the input to the error amplifier of channel 2. An external resistive divider connects FB2 between the output and ground. The voltage on FB2 is compared with the internal 0.6V reference to set the regulation voltage of channel 2.
6	7	AGND	Analog ground. Connect AGND to PGND1 and PGND2 externally on the board.
7	8	VCC	Power supply to the internal regulator for both channels. Decouple VCC with a 0.1 - 1 μ F capacitor between VCC and AGND.
8	9	CCM	AAM or forced CCM control. Pull CCM high to enter forced CCM mode. Pull CCM low to enter AAM mode at light load. Do not float CCM.
9	10	FB1	Feedback for channel 1. FB1 is the input to the error amplifier of channel 1. An external resistive divider connects FB1 between the output and GND. The voltage on FB1 is compared with the internal 0.6V reference to set the regulation voltage of channel 1.
10	11	SS1	Soft start for channel 1.
11	12	VIN1	Input supply for channel 1. Place a decoupling capacitor to ground close to VIN1 to reduce switching spikes.
12	13	SW1	Switch node connection to the inductor for channel 1. SW1 connects to the internal high- and low-side power MOSFET switches of the channel 1 buck.
13	14	PGND1	Power ground of channel 1. Connect PGND1 with larger copper areas to the negative terminals of the input and output capacitors. PGND1 must be connected to PGND2 on board externally.
14	15	PG1	Power good for channel 1.
15	16	EN1	Enable control for channel 1.
16	17	FREQ	Frequency set. Connect a resistor to GND to set the switching frequency. The switching frequency can be synchronized by an external clock via FREQ.
17	18	EN2	Enable control for channel 2.
18	1	PG2	Power good for channel 2.

ABSOLUTE MAXIMUM RATINGS (1)

Supply voltage (V _{IN})	6.5V
V _{SW}	-0.3V to V _{IN} + 0.3V
All other pins	-0.3V to +6.5V
Junction temperature	150°C
Lead temperature	260°C
Storage temperature	-65°C to 150°C
Continuous power dissipation (T _A = +25°C) (2)	
QFN-18 (2mmx3mm)	1.78W
QFN-18 (2.5mmx3.5mm)	2.5W

Recommended Operating Conditions

Supply voltage (V _{IN})	2.7V to 6V
Output voltage (V _{OUT})	0.6V to 5.5V
Operating junction temp.....	-40°C to +125°C

Thermal Resistance (3)	θ_{JA}	θ_{JC}
QFN-18 (2mmx3mm).....	70.....	15....°C/W
QFN-18 (2.5mmx3.5mm).....	50.....	12....°C/W

NOTES:

- 1) Exceeding these ratings may damage the device.
- 2) The maximum allowable power dissipation is a function of the maximum junction temperature T_J (MAX), the junction-to-ambient thermal resistance θ_{JA}, and the ambient temperature T_A. The maximum allowable continuous power dissipation at any ambient temperature is calculated by P_D (MAX) = (T_J (MAX)-T_A)/θ_{JA}. Exceeding the maximum allowable power dissipation produces an excessive die temperature, causing the device to go into thermal shutdown. Internal thermal shutdown circuitry protects the device from permanent damage.
- 3) Measured on JESD51-7, 4-layer PCB.

ELECTRICAL CHARACTERISTICS

$V_{IN} = 5V$, $T_J = -40^{\circ}C$ to $+125^{\circ}C$, unless otherwise noted. Typical values are at $T_J = 25^{\circ}C$.

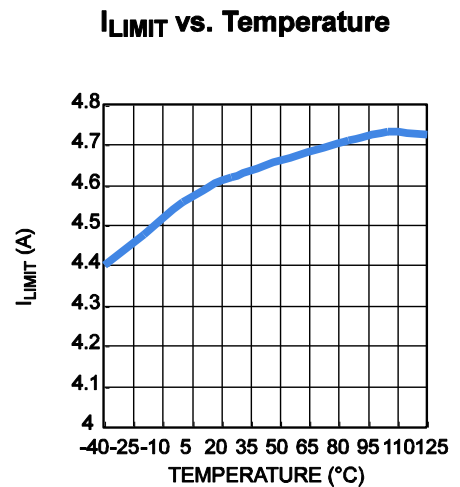
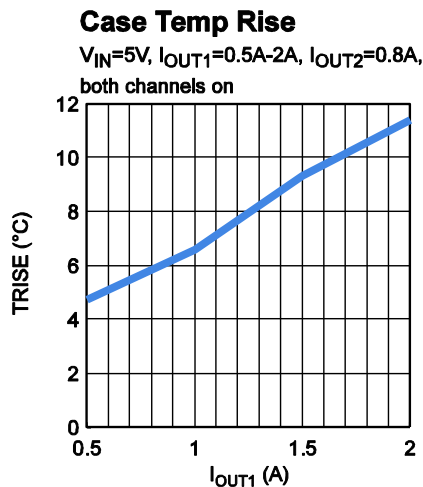
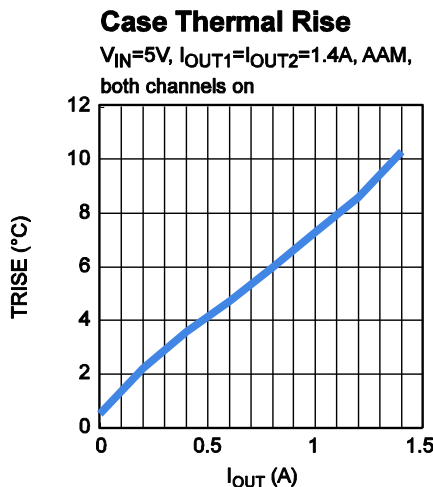
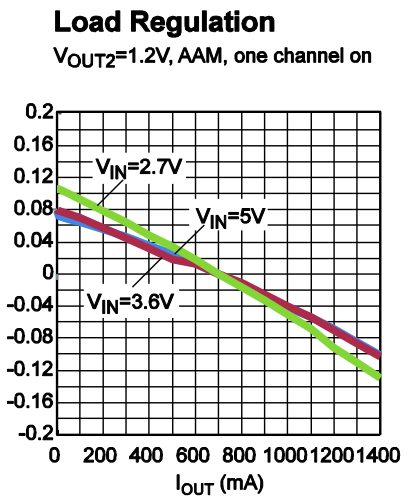
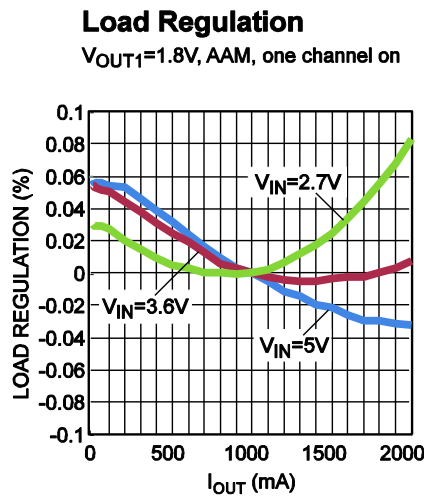
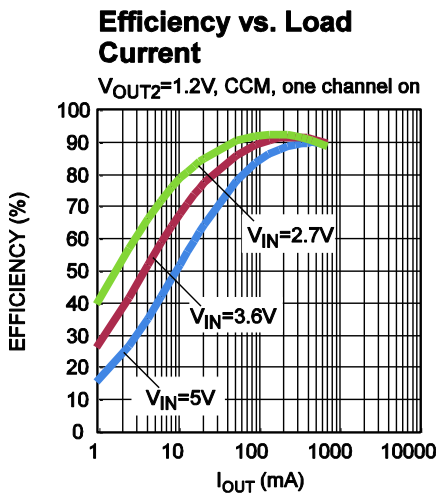
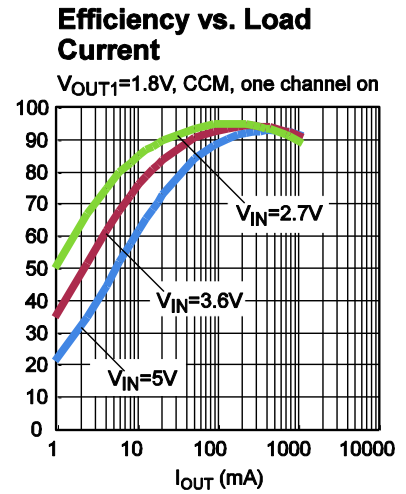
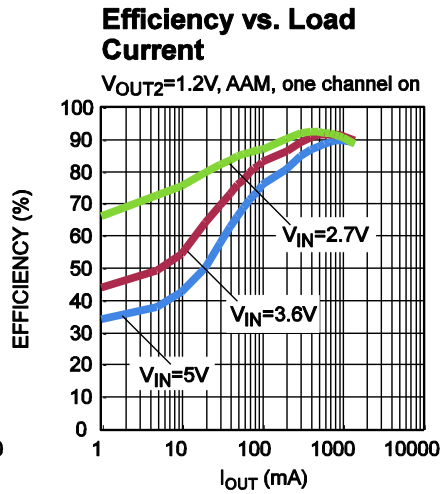
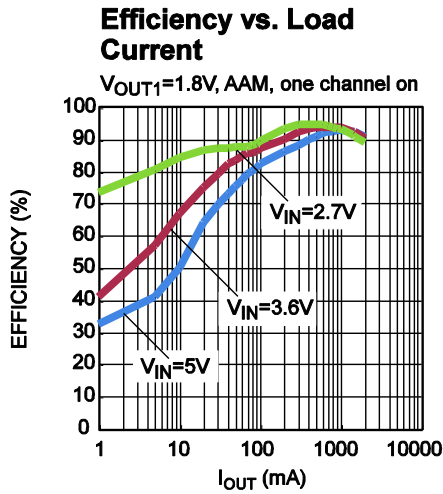
Parameters	Symbol	Condition	Min	Typ	Max	Units
Supply current (quiescent)	I_Q	$V_{IN} = 5V$, $V_{EN} = 2V$, $V_{FB} = 0.65V$, no switching		60	80	μA
Shutdown current	I_{SHDN}	$V_{EN} = 0V$, CCM = GND, $T_J = 25^{\circ}C$		0	0.2	μA
		$V_{EN} = 0V$, CCM=GND, $T_J = -40^{\circ}C$ to $+85^{\circ}C$ ⁽⁴⁾		0	1.5	μA
		$V_{EN} = 0V$, CCM = GND, $T_J = +85^{\circ}C$ to $+125^{\circ}C$			5	μA
V_{IN} under-voltage lockout threshold	$I_{N_{UVLO}}$	Rising edge		2.4	2.55	V
V_{IN} under-voltage lockout hysteresis	$I_{N_{UVLO_HYS}}$			230		mV
Regulated FB voltage	V_{FB}	$T_J = +25^{\circ}C$	0.593	0.600	0.607	V
		$T_J = -40^{\circ}C$ to $+125^{\circ}C$	0.588	0.600	0.612	V
FB input current	I_{FB}	$V_{FB} = 0.65V$		0	50	nA
EN high threshold	V_{EN_H}		1.6			V
EN low threshold	V_{EN_L}				0.4	V
EN input current	I_{EN}	$V_{EN} = 2V$		0	0.1	μA
		$V_{EN} = 0V$		0	0.1	μA
HS switch on resistance	R_{DSON_P}	$V_{IN} = 5V$		60	90	m Ω
LS switch on resistance	R_{DSON_N}	$V_{IN} = 5V$		25	45	m Ω
SW leakage current	I_{SW_LK}	$V_{EN} = 0V$, $V_{IN} = 6V$, $V_{SW} = 0V$ and $6V$, $T_J = 25^{\circ}C$	-1	0	1	μA
HS switch current limit ⁽⁴⁾	I_{HS_LIMIT}	Sourcing	3.0	4.0	5.6	A
LS valley current limit ⁽⁴⁾	I_{VALLEY}			3.4		A
LS switch current limit	I_{LS_LIMIT}	Sinking, CCM	1			A
Oscillator frequency accuracy	f_{SW}	$R_{FREQ} = 665k\Omega$	298	350	402	kHz
		$R_{FREQ} = 200k\Omega$	850	1000	1150	kHz
		$R_{FREQ} = 51k\Omega$	2700	3000	3300	kHz
Sync frequency range	f_{SYNC}		0.35		3	MHz
Phase shift				180		$^{\circ}$
Minimum on time ⁽⁴⁾	T_{ON_MIN}			55		ns
Minimum off time ⁽⁴⁾	T_{OFF_MIN}			50		ns
Maximum duty cycle	D_{MAX}			100		%
Thermal shutdown threshold ⁽⁴⁾	T_D			175		$^{\circ}C$
Thermal shutdown hysteresis ⁽⁴⁾	T_{D_HYS}			40		$^{\circ}C$
Soft-start charging current	I_{SS}	$V_{SS} = 0V$	2	3.2	5	μA
Power good rising threshold	$PGOOD_{V_{th-Hi}}$		0.85	0.9	0.95	V_{FB}
Power good falling threshold	$PGOOD_{V_{th-Lo}}$		0.77	0.82	0.87	V_{FB}
Power good threshold hysteresis	$PGOOD_{V_{th-Hys}}$			0.08		V_{FB}
Power good rising delay	T_{PGOOD_R}			30		μs
Power good falling delay	T_{PGOOD_F}			40		μs
CCM on threshold			1.6			V
CCM off threshold					0.4	V

NOTE:

4) Not tested in production and guaranteed by design and characterization.

TYPICAL PERFORMANCE CHARACTERISTICS

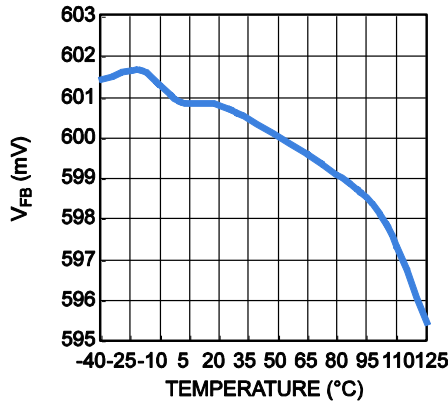
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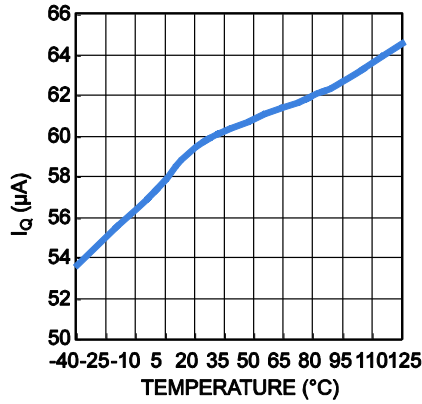
TYPICAL PERFORMANCE CHARACTERISTICS (continued)

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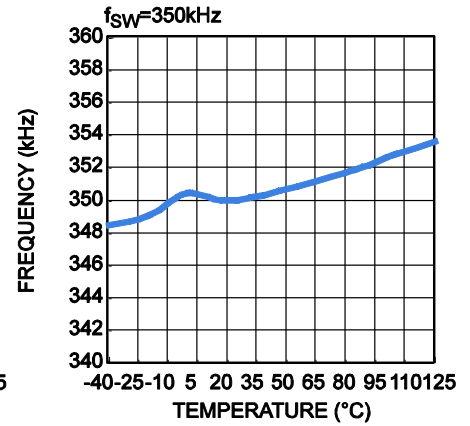
V_{FB} vs. Temperature



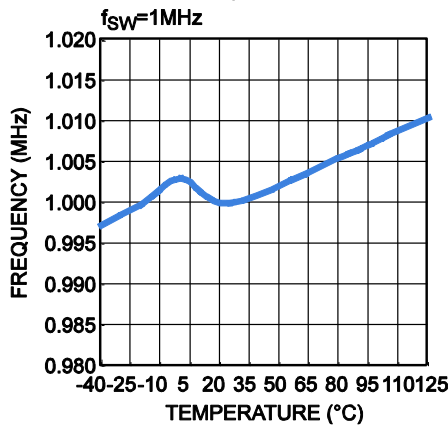
I_Q vs. Temperature



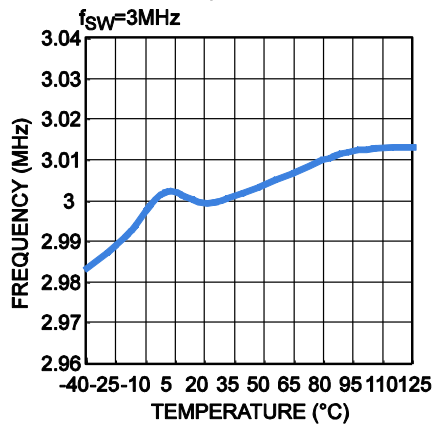
Frequency vs. Temperature



Frequency vs. Temperature

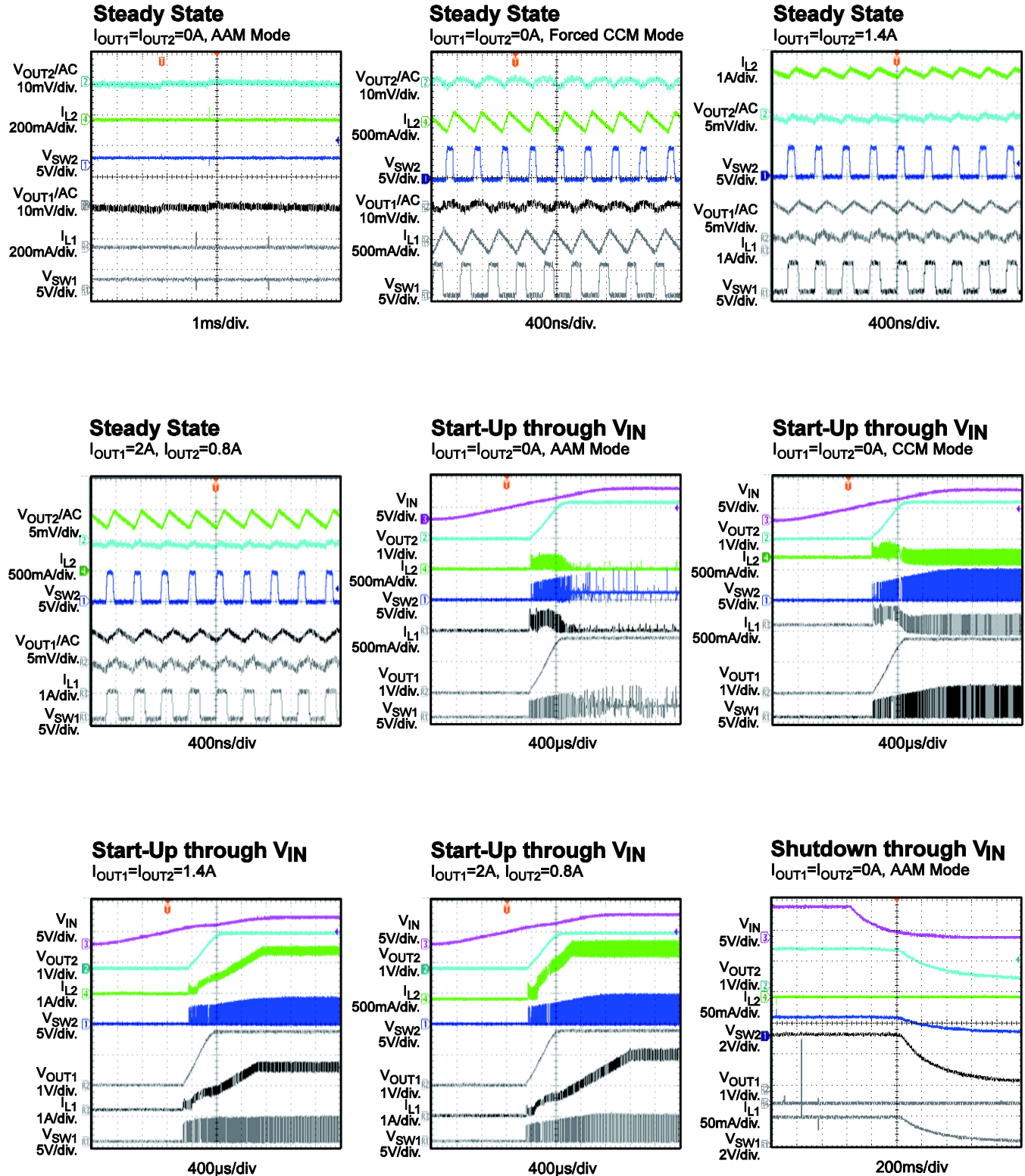


Frequency vs. Temperature



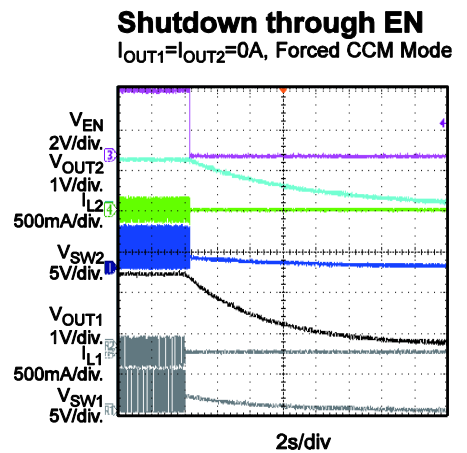
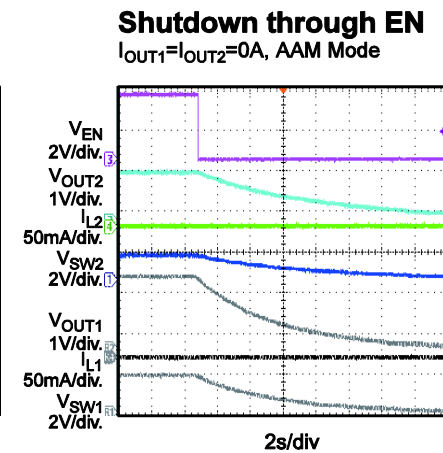
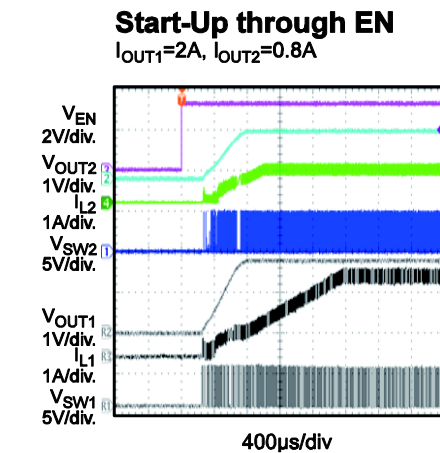
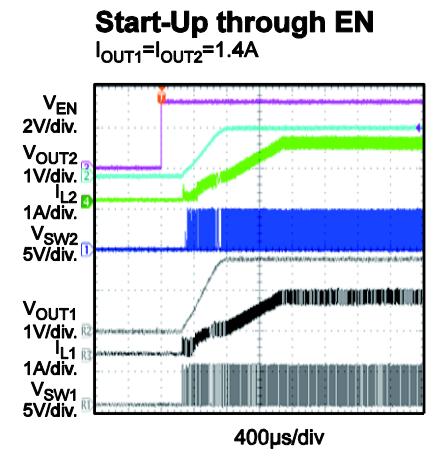
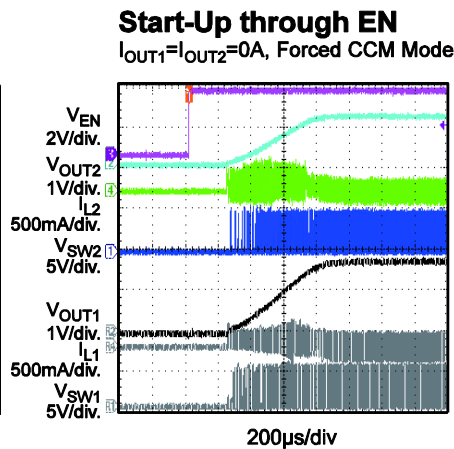
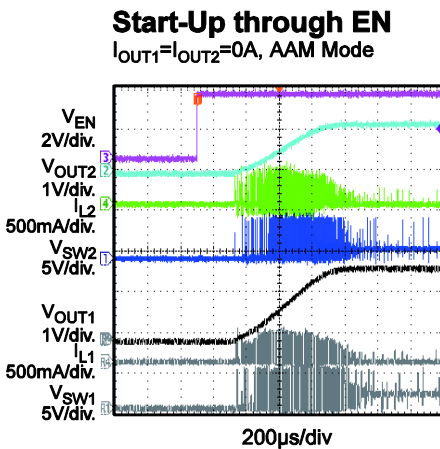
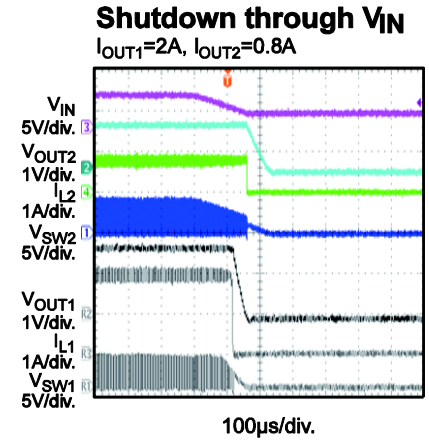
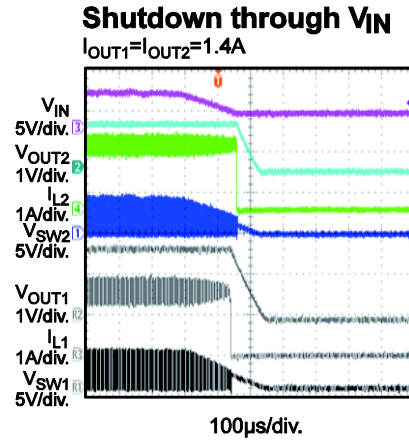
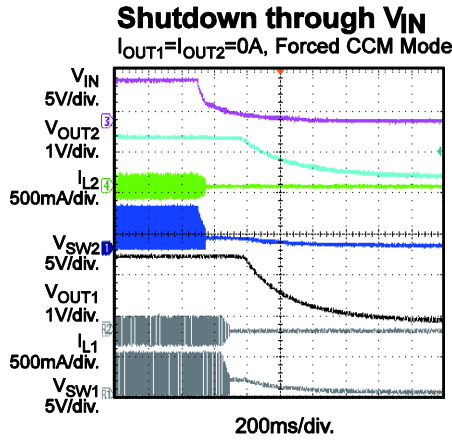
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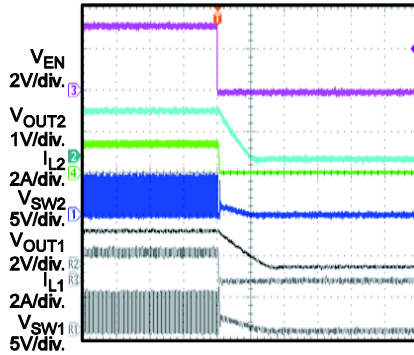
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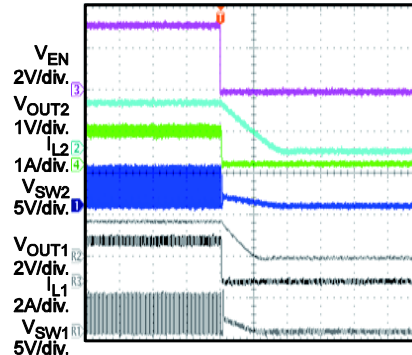
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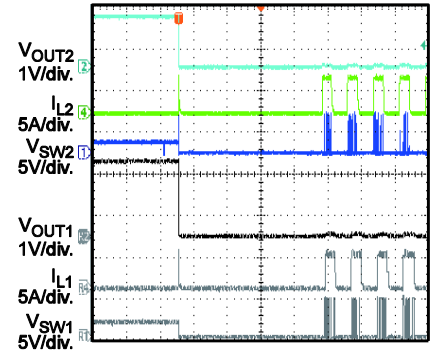


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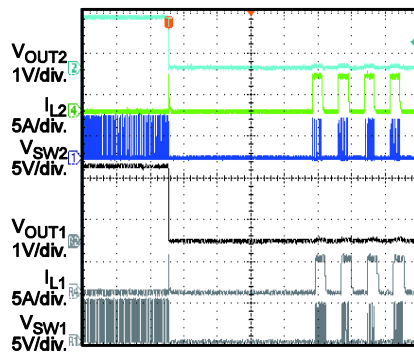
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Shutdown through EN
 $I_{OUT1}=I_{OUT2}=1.4A$

 40 μs /div.

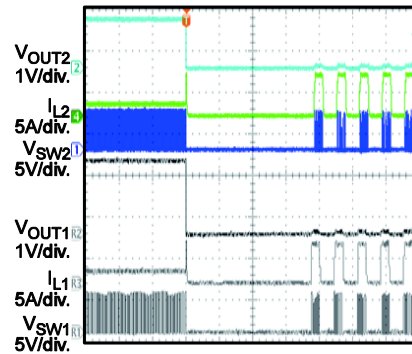
Shutdown through EN
 $I_{OUT1}=2A$, $I_{OUT2}=0.8A$

 40 μs /div.

SCP Entry
 $I_{OUT1}=I_{OUT2}=0A$, AAM Mode


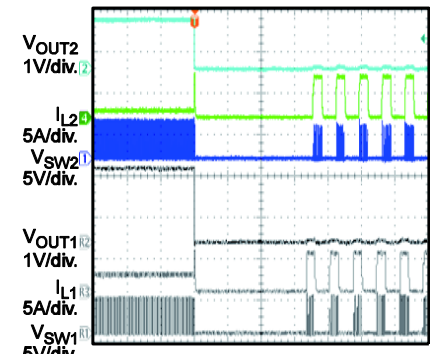
2ms/div.

SCP Entry
 $I_{OUT1}=I_{OUT2}=0A$, Forced CCM Mode


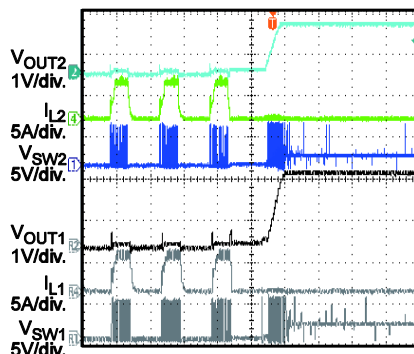
2ms/div

SCP Entry
 $I_{OUT1}=I_{OUT2}=1.4A$


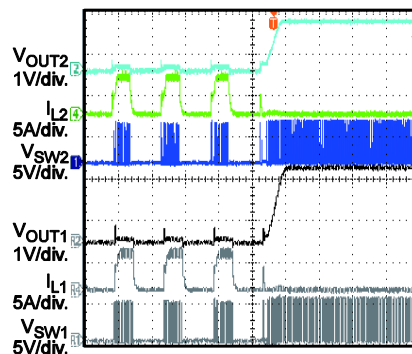
2ms/div

SCP Entry
 $I_{OUT1}=2A$, $I_{OUT2}=0.8A$


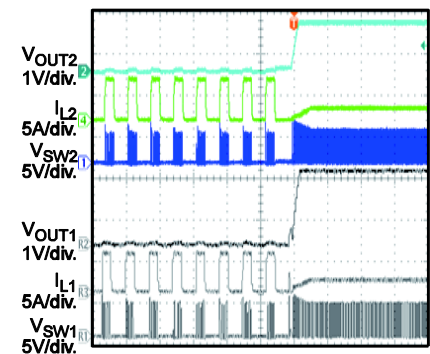
2ms/div

SCP Recovery
 $I_{OUT1}=I_{OUT2}=0A$, AAM Mode


1ms/div

SCP Recovery
 $I_{OUT1}=I_{OUT2}=0A$, Forced CCM Mode


1ms/div

SCP Recovery
 $I_{OUT1}=I_{OUT2}=1.4A$


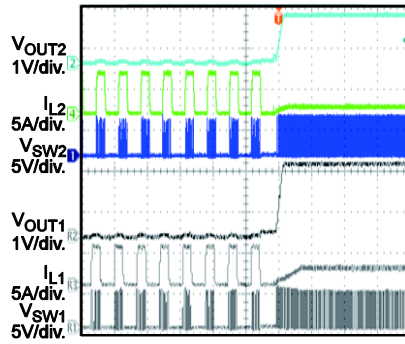
2ms/div

TYPICAL PERFORMANCE CHARACTERISTICS (continued)

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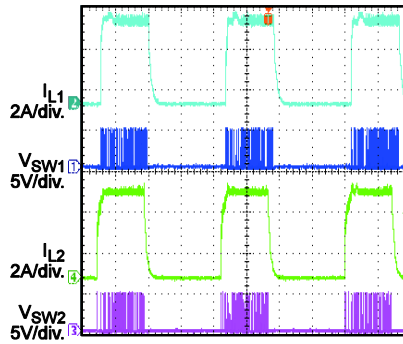
SCP Recovery

$I_{OUT1}=2A$, $I_{OUT2}=0.8A$



2ms/div.

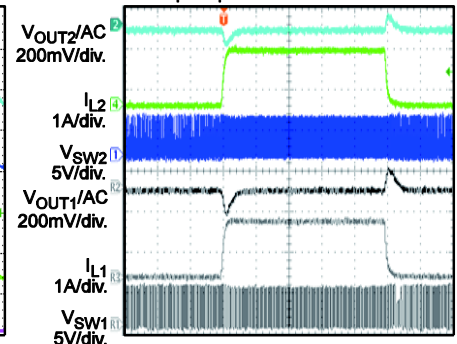
SCP Steady State



400µs/div.

Load Transient

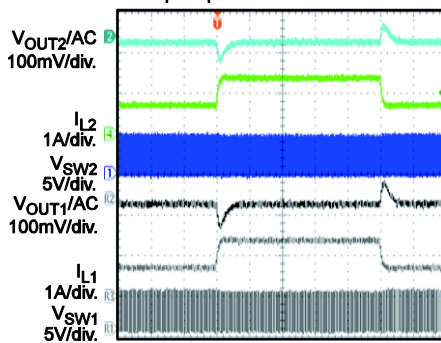
$I_{OUT1}=I_{OUT2}=0$ to 1.4A, AAM Mode, 1.6A/µs Speed



100µs/div.

Load Transient

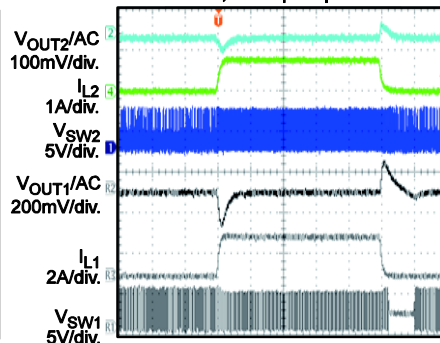
$I_{OUT1}=I_{OUT2}=0.7$ to 1.4A, 1.6A/µs Speed



100µs/div

Load Transient

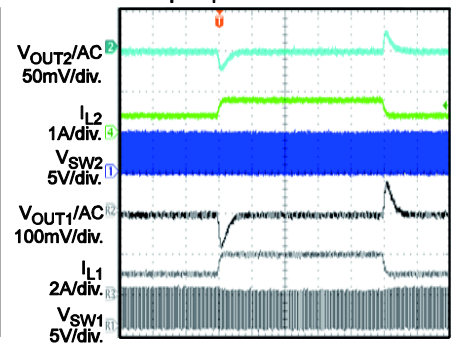
$I_{OUT1}=0$ to 2A, $I_{OUT2}=0$ to 0.8A, AAM Mode, 1.6A/µs Speed



100µs/div

Load Transient

$I_{OUT1}=1$ to 2A, $I_{OUT2}=0.4$ to 0.8A, 1.6A/µs Speed



100µs/div

BLOCK DIAGRAM

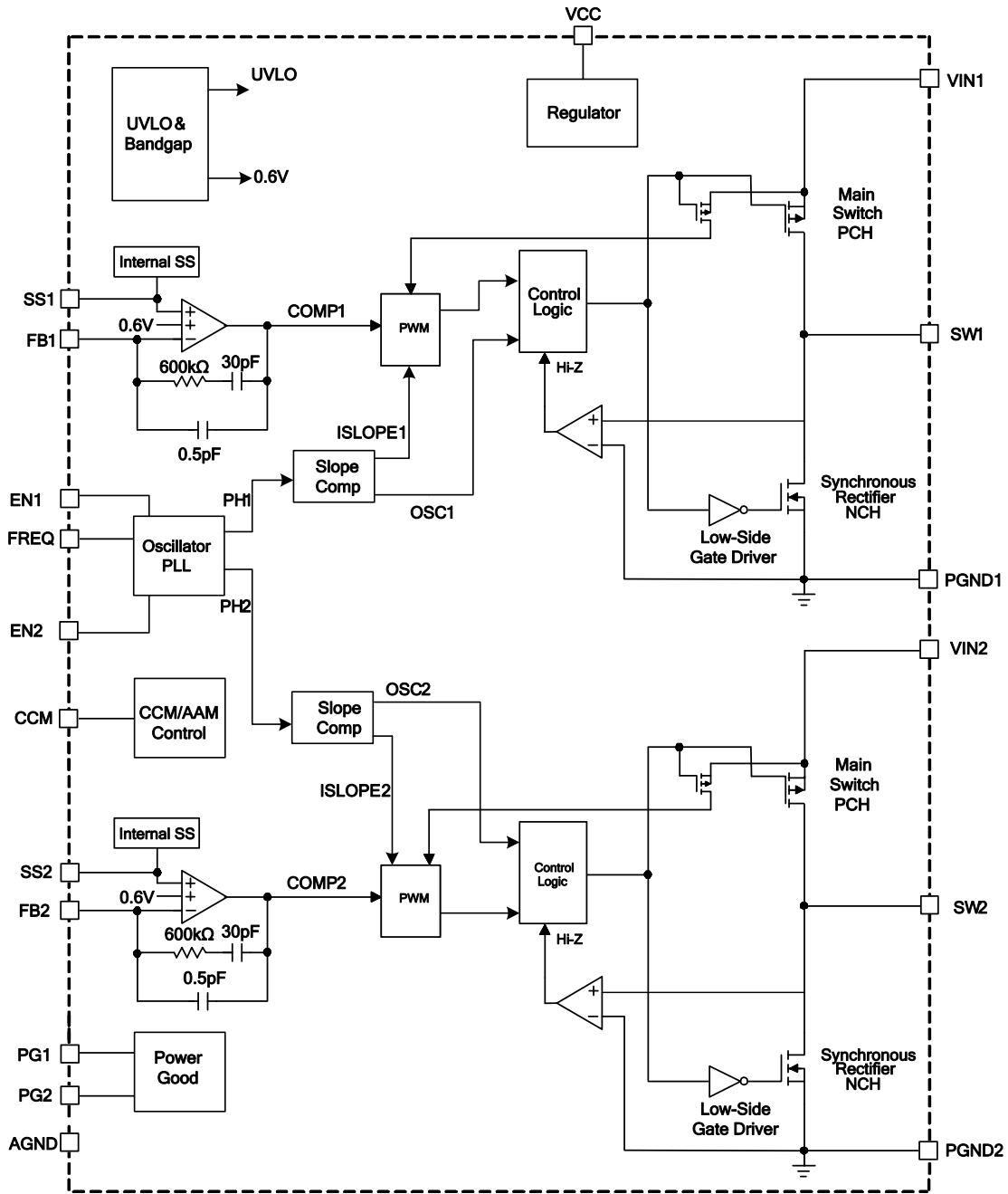


Figure 1: Functional Block Diagram

OPERATION

The MPQ2169 is a fully integrated, dual-channel, synchronous, step-down converter. Both channels use peak-current-mode control with internal compensation for fast transient response and cycle-to-cycle current limiting.

The MPQ2169 is optimized for low-voltage, portable applications where efficiency and small size are critical.

180° Out-of-Phase Operation

The MPQ2169 operates the two channels in 180° out-of-phase operation to reduce the input current ripple, so a smaller input bypass capacitor can be used. When both channels operate in continuous conduction mode (CCM), two internal clocks are used (see Figure 2). The high-side MOSFET (HS-FET) is turned on at the clock's rising edge of the corresponding channel.

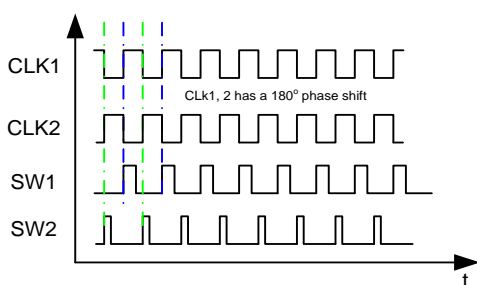


Figure 2: 180° Out-of-Phase Operation

At low dropout mode, when the switching frequency is stretched out for each channel, the MPQ2169 runs at a fixed off time with its own independent switching frequency. After the input voltage rises high again, frequency stretch mode ends, and pulse-width modulation (PWM) mode resumes and synchronizes with the master oscillator for out-of-phase operation.

Light-Load Operation

In light-load condition, the MPQ2169 can work in two different operating modes by setting CCM to different statuses.

The MPQ2169 works in forced continuous conduction mode (FCCM) when the CCM pin is pulled above 1.6V. The MPQ2169 works with a fixed frequency from no load to full load in this mode. The advantage of CCM is the controllable frequency and lower output ripple at light load.

The shutdown current in FCCM (50μA at 3.3V) is much higher than that in advanced asynchronous mode (AAM) due to some active internal circuits. It is recommended to pull CCM low when the MPQ2169 has been shut down due to a high shutdown current.

The MPQ2169 works in AAM when CCM is pulled below 0.4V. AAM is used to optimize efficiency during light-load and no-load conditions.

When AAM is enabled, the MPQ2169 first enters non-synchronous operation as the inductor current approaches zero at light load. If the load decreases further or is at no load, which makes the internal COMP voltage (V_{COMP}) decrease to the set value, then the MPQ2169 enters AAM. In AAM, the internal clock is reset whenever V_{COMP} crosses over the set value, and the crossover time is taken as the benchmark of the next clock. When the load increases and V_{COMP} is higher than the set value, the operation mode is in CCM or discontinuous conduction mode (DCM), which have a constant switching frequency.

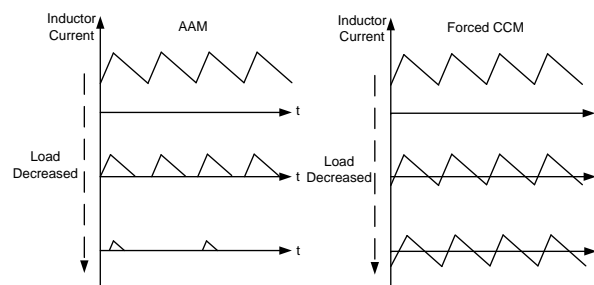


Figure 3: AAM and Forced CCM

Soft Start (SS)

The MPQ2169 has a built-in soft start that ramps up the output voltage at a controlled slew rate, preventing an overshoot at start-up. The soft-start time is about 0.5ms, typically.

The soft-start time can also be programmed by an external capacitor connected to SS, shown in Equation (1):

$$t_{SS}(\text{ms}) = \frac{C_{SS}(\text{nF}) \times V_{RFF}(\text{V})}{I_{SS}(\mu\text{A})} \quad (1)$$

Where C_{SS} is the external SS capacitor, V_{REF} is the internal reference voltage (0.6V), and I_{SS} is the 3.2 μ A SS charge current.

Oscillator and Sync Function

The internal oscillator frequency is set by a single external resistor (R_{FREQ}) connected between FREQ and ground. The frequency-setting resistor should be located close to the device. The relationship between the oscillator frequency and R_{FREQ} is shown in Figure 4.

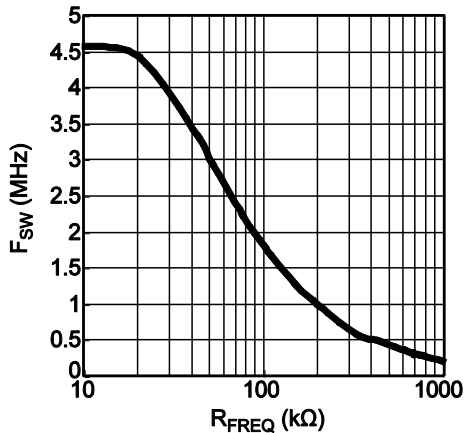


Figure 4: F_{sw} vs. R_{FREQ}

FREQ can also be used to synchronize the internal oscillator to an external clock. The rising edge of the channel 1 clock is synchronized to the external clock's rising edge, while the channel 2 clock remains at 180° out-of-phase to channel 1. The recommended external SYNC frequency is in the range of 350kHz to 3MHz. While there is no pulse width requirement, note that there is always parasitic capacitance of the pad there, so if the pulse width is too short, a clear rising and falling edge may not be seen. The pulse is recommended to be longer than 100ns.

Power Good (PG)

The MPQ2169 has one power good (PG) output to indicate normal operation after the soft-start time. PG is the open drain of an internal MOSFET. It should be connected to VIN, VCC, or an external voltage source through a resistor (i.e.: 100k Ω). After the input voltage is applied, the MOSFET is turned on and PG is pulled to GND before SS is ready. After the FB voltage (V_{FB}) reaches 90% of the reference voltage (V_{REF}), the MOSFET turns off and PG is pulled high by an external voltage source. When V_{FB} drops to 82% of V_{REF} , the PG voltage is pulled to GND to indicate a failure output.

Current Limit and Short Circuit

Each channel of the MPQ2169 has a typical 4A current limit for the high-side switch. When FB drops to 60% of the reference value and SS is sufficient, the MPQ2169 treats this as a short and attempts to recover with hiccup mode.

In hiccup mode, the MPQ2169 disables the output power stage, slowly discharges the soft-start cap, and soft starts automatically. If the short-circuit condition still remains, the MPQ2169 repeats this operation cycle until the short circuit is removed and the output rises back to regulation levels.

Dropout Operation

The MPQ2169 allows the high-side switch to remain on for more than one switching cycle and increases the duty cycle while the input voltage drops down to the output voltage. When the duty cycle reaches 100%, the high-side switch turns on to deliver current to the output up to its current limit. The output voltage is then the difference between the input voltage, the voltage drop across the main switch, and the inductor.

APPLICATION INFORMATION

Setting the Output Voltage

The external resistor divider sets the output voltage. The feedback resistor (R1) also sets the feedback loop bandwidth with the internal compensation. The T-type network is recommended (see Figure 5).

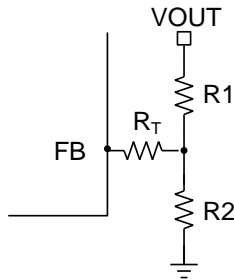


Figure 5: T-Type Feedback Network

$R_T + R1$ is used to set the loop bandwidth. The lower $R_T + R1$ is, the higher the bandwidth will be. However, a high bandwidth may cause an insufficient phase margin, resulting in loop instability. Therefore, a proper R_T value is required to make a trade-off between the bandwidth and phase margin. Table 1 lists the recommended feedback resistor and R_T values for various output voltages.

R1 is estimated to be 100k Ω . R2 can then be calculated with Equation (2):

$$R2 = \frac{R1}{\frac{V_{OUT}}{0.6V} - 1} \quad (2)$$

Table 1: Resistor Selection vs. Output Voltage Setting

V _{OUT}	R _T	R1	R2
1.2V	100k Ω	100k Ω	100k Ω
1.5V	100k Ω	100k Ω	66.5k Ω
1.8V	100k Ω	100k Ω	49.9k Ω
2.5V	100k Ω	100k Ω	31.6k Ω
3.3V	100k Ω	100k Ω	22.1k Ω

In the case of ceramic capacitors used as output capacitors (C_O), the feedback loop bandwidth (f_c) is no higher than 1/10 of the switching frequency for optimal transient performance and good phase margin. If an electrolytic capacitor is used, the loop bandwidth is no higher than 1/4 of the ESR zero frequency (f_{ESR}).

f_{ESR} can be calculated by Equation (3):

$$f_{ESR} = \frac{1}{2\pi \times R_{ESR} \times C_O} \quad (3)$$

For example, choose $f_c = 80\text{kHz}$ with a ceramic capacitor and $C_O = 22\mu\text{F}$.

Selecting the Inductor

An inductor with a DC current rating at least 25% higher than the maximum load current is recommended for most applications. For the best efficiency, the inductor DC resistance should be less than 20m Ω . For most designs, the inductance value can be derived from Equation (4):

$$L = \frac{V_{OUT} \times (V_{IN} - V_{OUT})}{V_{IN} \times \Delta I_L \times f_{SW}} \quad (4)$$

Where ΔI_L is inductor ripple current. Choose the inductor ripple current to be approximately 30% of the maximum load current.

The maximum inductor peak current can be calculated with Equation (5):

$$I_{L(MAX)} = I_{LOAD} + \frac{\Delta I_L}{2} \quad (5)$$

Selecting the Input Capacitor

The input capacitor reduces the surge current drawn from the input and the switching noise from the device. The input capacitor impedance at the switching frequency should be less than the input source impedance to prevent high-frequency switching current from passing to the input source. Ceramic capacitors with X5R or X7R dielectrics are highly recommended because of their low ESR and small temperature coefficients. For most applications, a 22 μF capacitor is sufficient.

Selecting the Output Capacitor

The output capacitor (C_O) keeps the output voltage ripple small and ensures a stable regulation loop. The output capacitor impedance should be low at the switching frequency. Use ceramic capacitors with X5R or X7R dielectrics. If an electrolytic capacitor is used, pay close attention to the output ripple voltage, extra heating, and the selection of the upper feedback resistor because of the large ESR of electrolytic capacitor (refer to the

Setting the Output Voltage section). The output ripple (ΔV_{OUT}) can be approximated with Equation (6):

$$\Delta V_{OUT} = \frac{V_{OUT} \times (V_{IN} - V_{OUT})}{V_{IN} \times L \times f_{SW}} \times \left(ESR + \frac{1}{8 \times f_{SW} \times C_o} \right) \quad (6)$$

Power Dissipation

IC power dissipation is important in circuit design, not only because of efficiency concerns, but also because of the chip's thermal requirements. Several parameters influence power dissipation, such as conduction loss (Cond), dead time (DT), switching loss (SW), MOSFET driver current (DR), and supply current (S).

Based on these parameters, estimate the power loss with Equation (7):

$$P_{LOSS} = P_{Cond} + P_{DT} + P_{SW} + P_{DR} + P_S \quad (7)$$

Thermal Regulation

Changes in the IC temperatures change the electrical characteristics, especially when the temperature exceeds the IC's recommended operating range. Managing the IC's temperature requires additional considerations to ensure that the IC runs within the maximum allowable temperature junction. Specific layout designs can improve the thermal profile while limiting costs to either the efficiency or operating range.

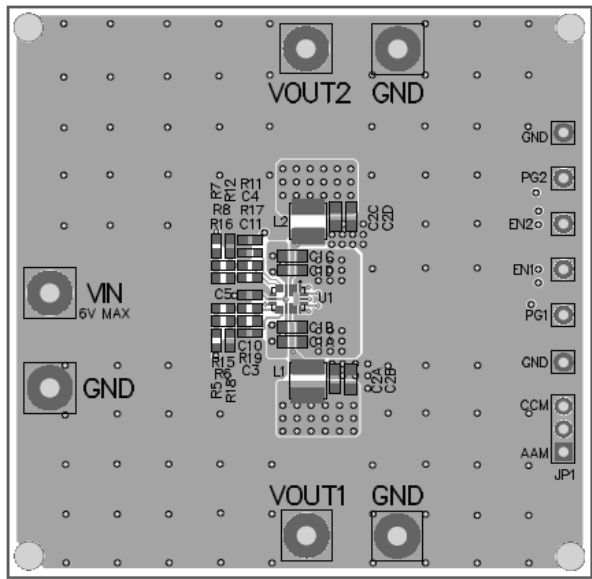
For the MPQ2169, connect the ground pin on the package to a ground plane on top of the PCB to use the plane as a heat sink. Connect this ground plane to the ground planes beneath the IC using vias to improve heat dissipation. Since these ground planes can introduce unwanted EMI noise and occupy valuable PCB space, design their size and shape to match the thermal resistance requirement.

Connecting the ground pin to a heat sink does not guarantee that the IC will not exceed its recommended temperature limits (i.e.: the ambient temperature exceeds the IC's temperature limits). If the ambient air temperature approaches the IC's temperature limit, the IC can be de-rated to operate using less power and help prevent thermal damage and unwanted electrical characteristics.

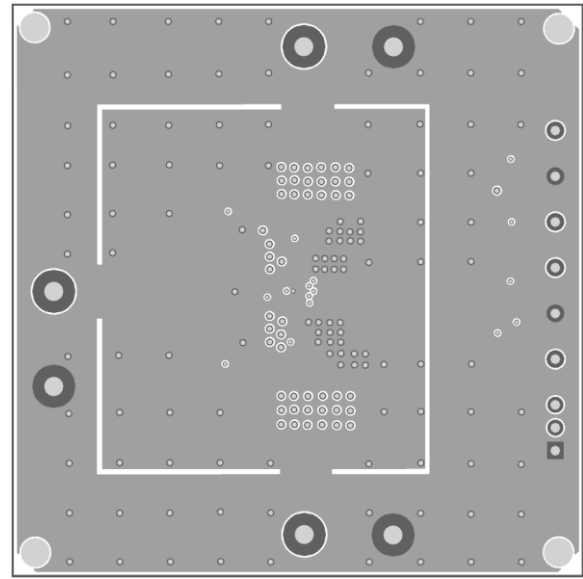
PCB Layout Guidelines ⁽⁵⁾

Efficient PCB layout is critical for stable operation. A four-layer layout is strongly recommended to achieve better thermal performance. For best results, refer to Figure 6 and follow the guidelines below.

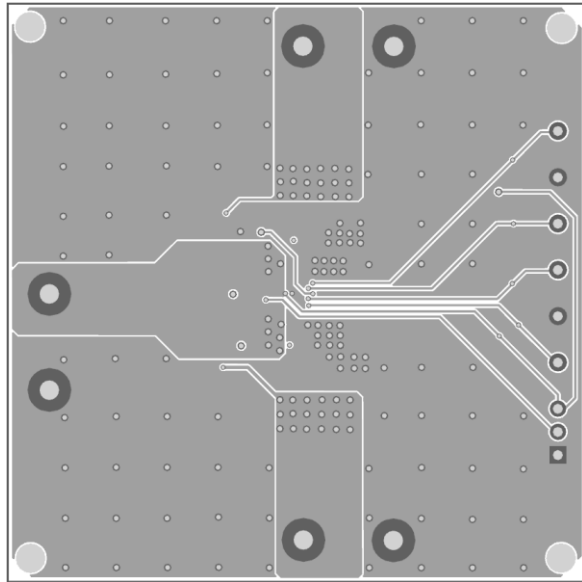
1. Place the high-current paths (PGND, VIN, and SW) very close to the device with short, direct, and wide traces.
2. Place input capacitors on both VIN sides and as close to VIN and PGND as possible.
3. Place the decoupling capacitor as close to VCC and AGND as possible.
4. Keep the switching node SW short and away from the feedback network.
5. Place the external feedback resistors next to FB. Do not place vias on the FB trace.
6. Connect PGND to a large copper area to achieve better thermal performance.
7. PGND1, PGND2, and AGND must be connected together on board externally.



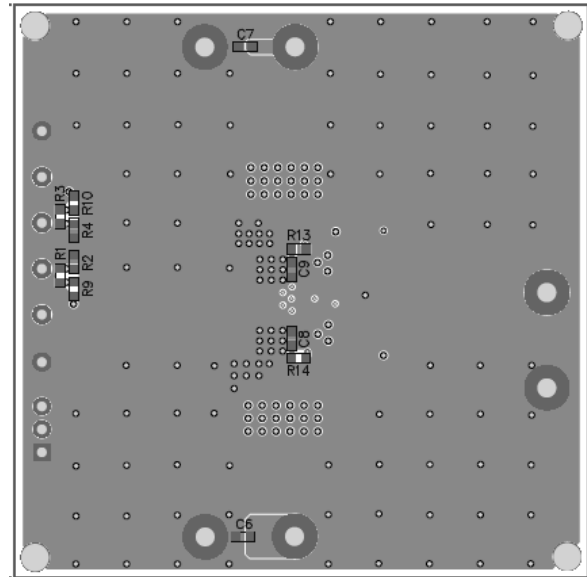
Top Layer



Inner Layer 1



Inner Layer 2



Bottom Layer

Figure 6: Recommended PCB Layout

NOTE:

5) The recommended PCB layout is based on Figure 7.

TYPICAL APPLICATION CIRCUITS

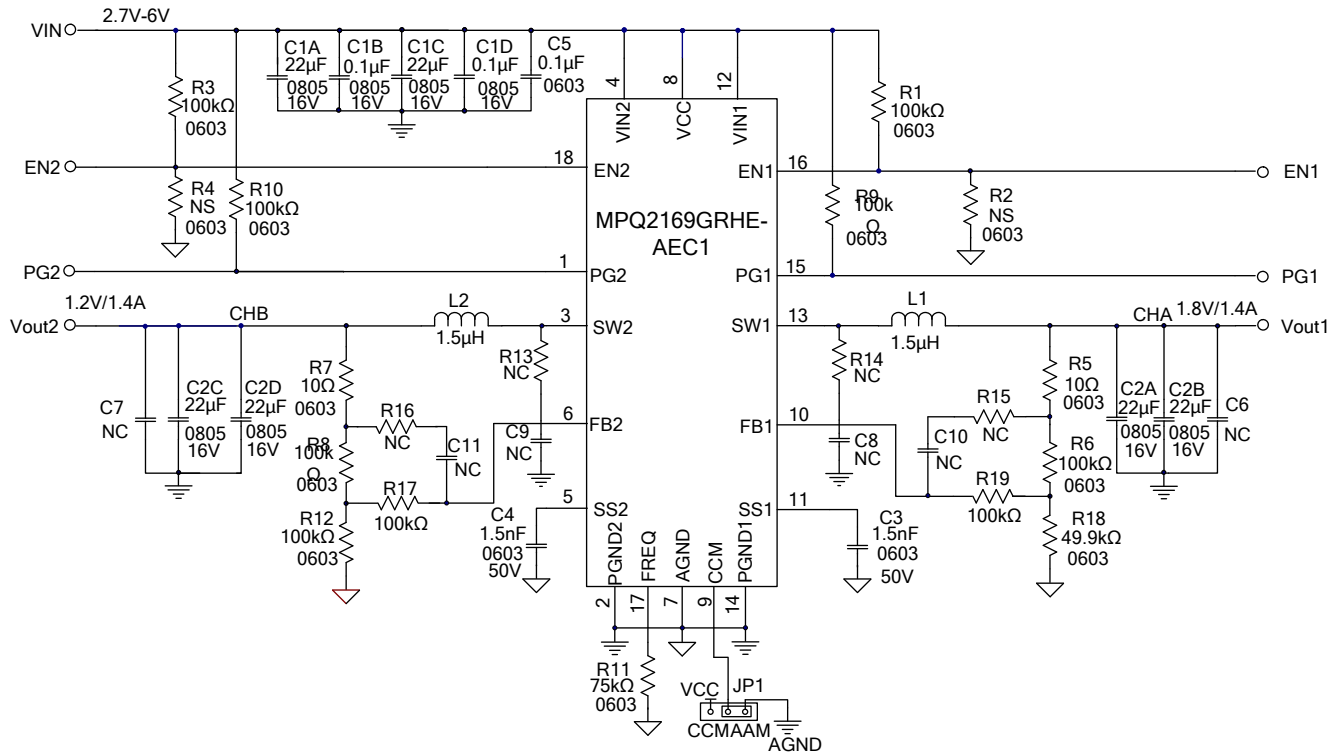


Figure 7: 1.4A/1.4A Application Circuit (MPQ2169GRHE-AEC1)

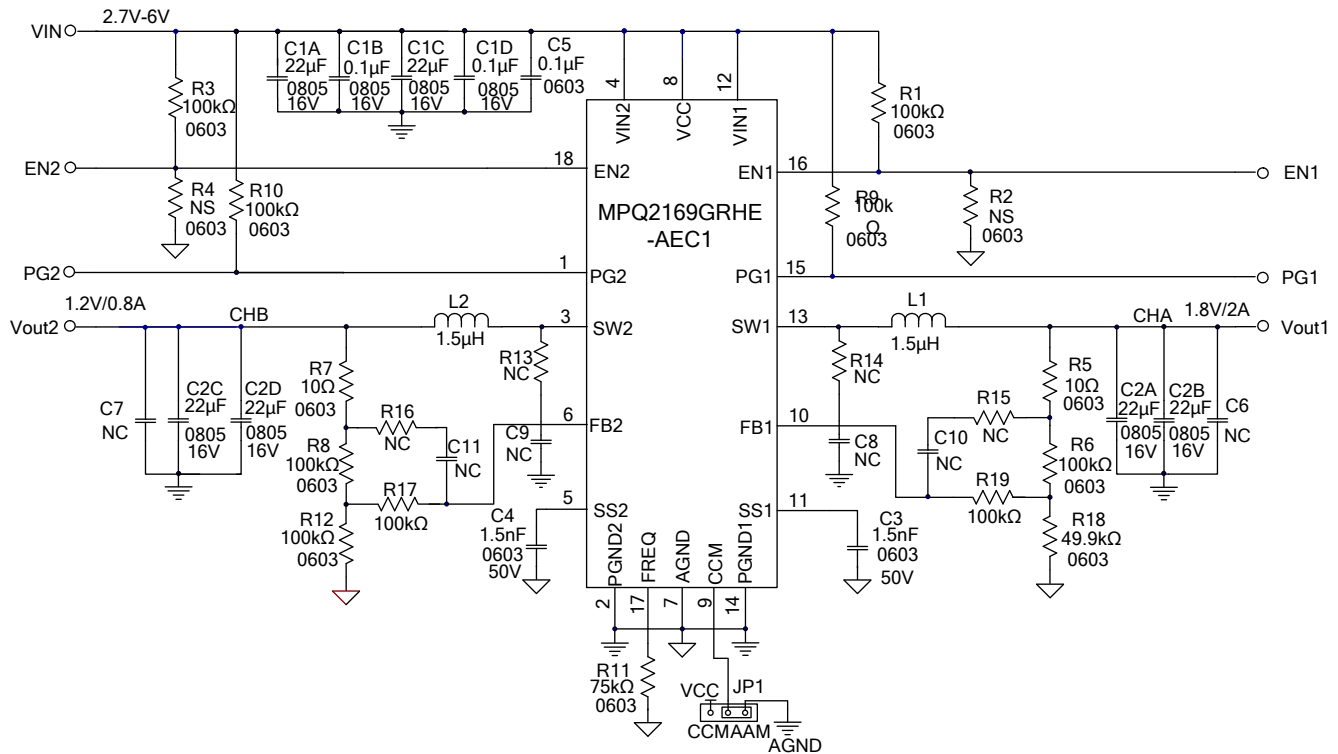


Figure 8: 2A/0.8A Application Circuit (MPQ2169GRHE-AEC1)

TYPICAL APPLICATION CIRCUITS (continued)

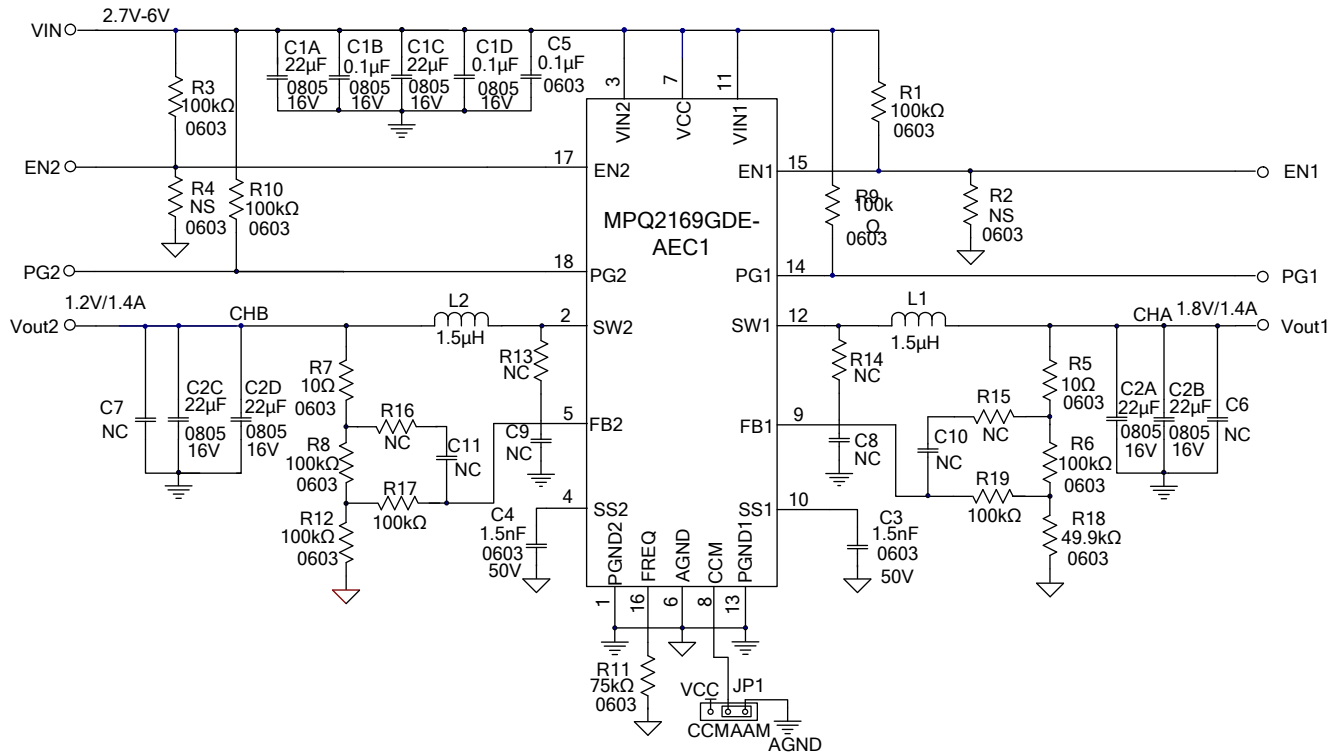


Figure 9: 1.4A/1.4A Application Circuit (MPQ2169GDE-AEC1)

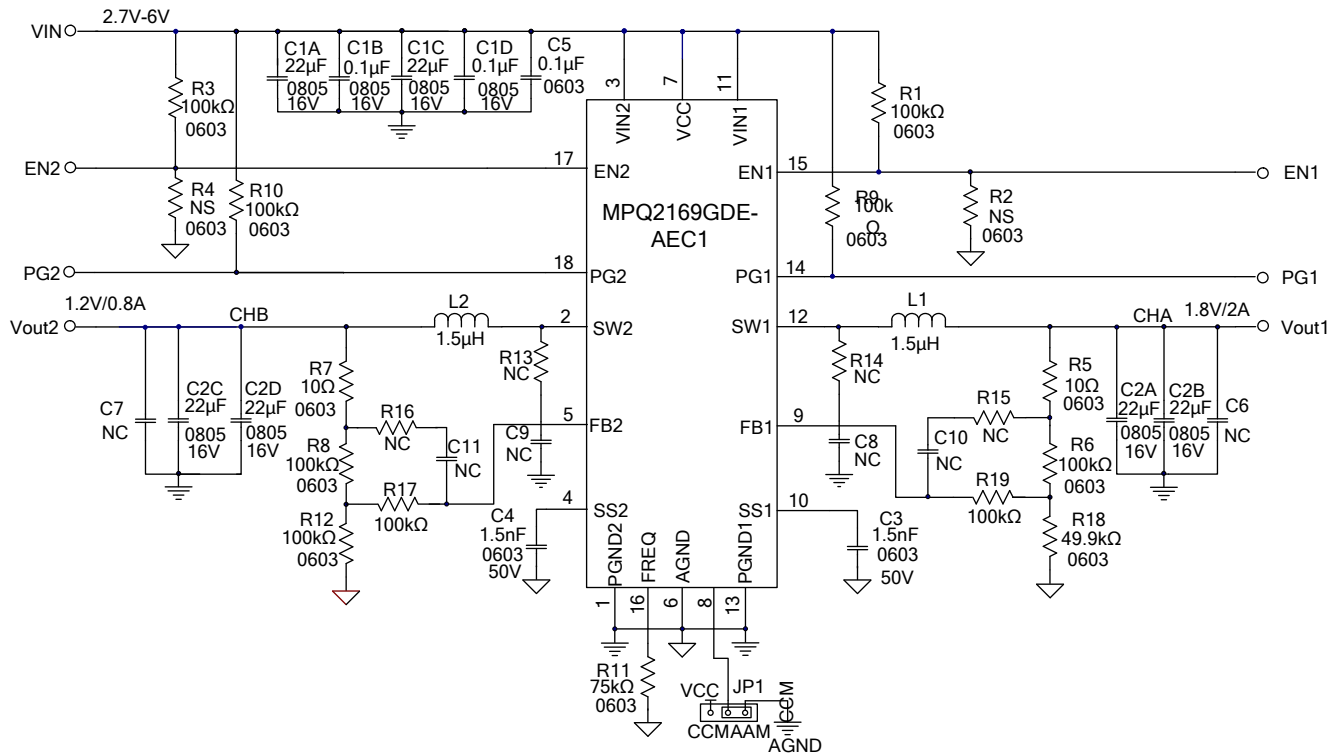
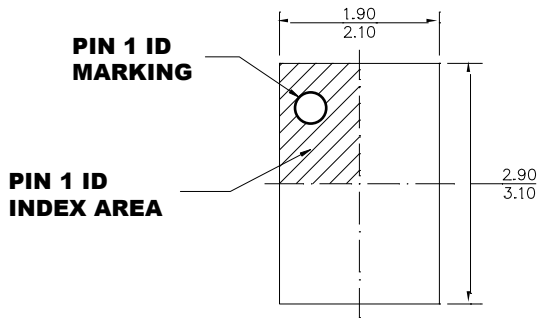


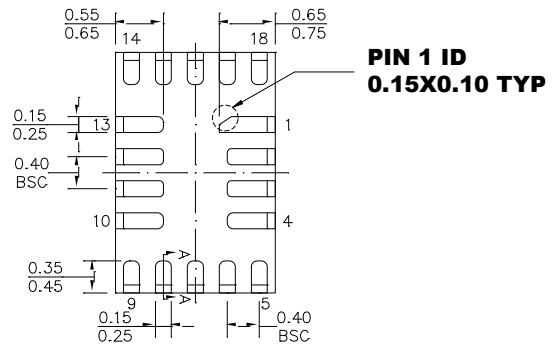
Figure 10: 2A/0.8A Application Circuit (MPQ2169GDE-AEC1)

PACKAGE INFORMATION

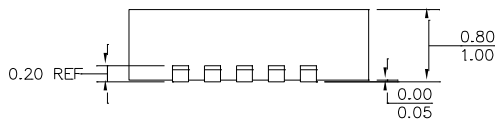
QFN-18 (2mmx3mm) Wettable Flank



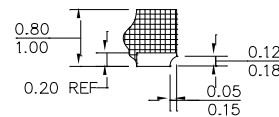
TOP VIEW



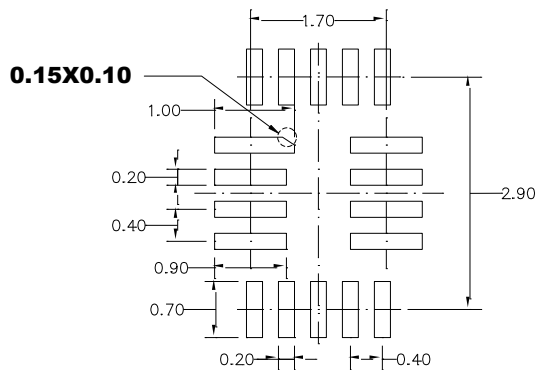
BOTTOM VIEW



SIDE VIEW



SECTION A-A



RECOMMENDED LAND PATTERN

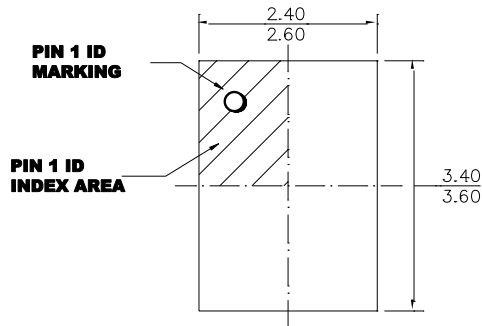
NOTE:

- 1) THE LEAD SIDE IS WETTABLE.
- 2) ALL DIMENSIONS ARE IN MILLIMETERS.
- 3) LEAD COPLANARITY SHALL BE 0.08 MILLIMETERS MAX.
- 4) JEDEC REFERENCE IS MO-220.
- 5) DRAWING IS NOT TO SCALE.

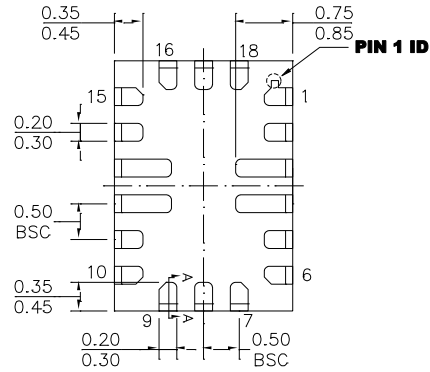
PACKAGE INFORMATION (continued)

QFN-18 (2.5mmx3.5mm)

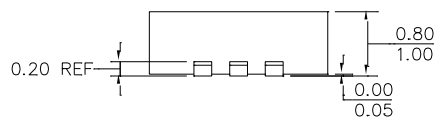
Wettable Flank



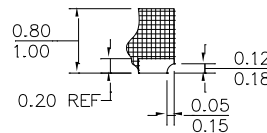
TOP VIEW



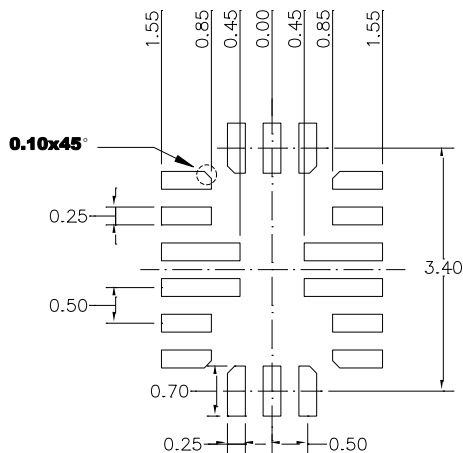
BOTTOM VIEW



SIDE VIEW



SECTION A-A



RECOMMENDED LAND PATTERN

NOTE:

- 1) THE LEAD SIDE IS WETTABLE.
- 2) LAND PATTERNS OF PIN3, 4, 12 AND 13 HAVE THE SAME LENGTH AND WIDTH.
- 3) ALL DIMENSIONS ARE IN MILLIMETERS.
- 4) LEAD COPLANARITY SHALL BE 0.08 MILLIMETERS MAX.
- 5) JEDEC REFERENCE IS MO-220.
- 6) DRAWING IS NOT TO SCALE.

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