# ISL15102IRZ-EVALZ <br> User's Manual: Evaluation Board 

Industrial Analog and Power

## 1. Overview

The ISL15102IRZ-EVAL board uses the ISL15102 single port differential line driver for Power Line Communication (PLC) applications. The device is designed to drive heavy line loads while maintaining a high level of linearity required in Orthogonal Frequency Division Multiplexing (OFDM) PLC modem links. The ISL15102IRZ-EVAL board has a disable control switch (DIS). In Disable mode, the line driver goes into Low Power mode and the outputs maintain a high impedance in the presence of high receive signal amplitude, improving TDM receive signal integrity. An internal input CM buffer maximizes the dynamic range and reduces the number of external components in the application circuit.

The ISL15102 is supplied in a thermally-enhanced small footprint ( 4 mmx 5 mm ) 24 Ld QFN package. The ISL15102 is specified for operation across the $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ ambient temperature range.

### 1.1 Key Features

- Single differential driver
- Internal $\mathrm{V}_{\mathrm{CM}}$
- 90 MHz signal bandwidth, $\mathrm{A}_{\mathrm{V}}=10, \mathrm{R}_{\mathrm{F}}=4.22 \mathrm{~K}$
- Single +8 V to +28 V supply, absolute maximum 30 V
- Supports narrowband and broadband DMT PLC
- Control switch to enable and disable TDM operation
- Fully assembled and tested


### 1.2 Specifications

This board has been configured and optimized for the following operating conditions:

- Single supply $\left(\mathrm{V}_{\mathrm{S}}=8\right.$ to 28 V$)$
- $\mathrm{A}_{\mathrm{V}}=10$
- $\mathrm{R}_{\mathrm{S}}=2.5 \Omega$
- AC coupled input and output


### 1.3 Recommended Equipment

The following materials are recommended to perform testing:

- 0 V to 28 V power supply with at least 1 A source current capability
- Resistive load capable of sinking current up to 1A
- Digital Multimeter (DMM)
- 100 MHz differential signal generator
- 100MHz quad-trace oscilloscope


### 1.4 Ordering Information

| Part Number | Description |
| :--- | :--- |
| ISL15102IRZ-EVALZ | Demonstration board with isolated outputs |

### 1.5 Block Diagram



Figure 1. Block Diagram

## 2. Functional Description

### 2.1 Quick Setup Guide

(1) Connect +12 V to the VS + plug and ground to the GND plug. The VS- plug is shorted to GND on the PCB and should remain unconnected.
(2) Turn on the power supply and place the DIS switch (SW1) to the GND (chip enabled) position. The supply current should be $\sim 23 \mathrm{~mA}$.
(3) Apply a -0.5 V to $+0.5 \mathrm{~V}\left(1 \mathrm{~V}_{\mathrm{P}-\mathrm{P}}\right) 1 \mathrm{MHz}$ differential sine wave signal to the INA and INB ports.
(4) Connect OUTA and OUTB to the high impedance inputs of the oscilloscope.
(5) Verify that the differential signal at OUTA and OUTB is sinusoidal and has an amplitude of -5 V to +5 V $\left(10 \mathrm{~V}_{\mathrm{P}-\mathrm{P}}\right)$ on the oscilloscope.

### 2.2 Switch Control

The ISL15102IRZ-EVAL board has a disable control switch (SW1). In Disable mode, the line driver goes into low power mode and the outputs maintain a high impedance in the presence of high receive signal amplitude, improving TDM receive signal integrity. Table 1 summarizes the switch settings.

Table 1. Switch Settings

| Switch Position | Function |
| :---: | :--- |
| GND | Driver enabled (DIS=0) |
| +5 V | Driver power-down (DIS=1). Output set to high impedance state |
| Center | DIS pin controlled by external signal through J1 |

### 2.3 Wideband Current Feedback Op Amps as Differential Drivers

A Current Feedback Amplifier (CFA), such as the ISL15102, is particularly suited to the requirements of high output power, high bandwidth, and differential drive. This topology offers a high slew rate on low quiescent power and the ability to hold AC characteristics relatively constant over a wide range of gains. The AC characteristics are principally set by the feedback resistor $\left(\mathrm{R}_{\mathrm{F}}\right)$ value in simple differential gain circuits as shown in Figure 1 on page 3.
In this differential gain of $10 \mathrm{~V} / \mathrm{V}$ circuit, the 4.22 k feedback resistors $\left(\mathrm{R}_{\mathrm{F}}\right)$ set the bandwidth, while the 931 gain resistor $\left(\mathrm{R}_{\mathrm{G}}\right)$ controls the gain. The $\mathrm{V}_{\mathrm{o}} / \mathrm{V}_{\mathrm{i}}$ gain for this circuit is set by (EQ. 1):
(EQ. 1) $\frac{\mathrm{V}_{\mathrm{o}}}{\mathrm{V}_{\mathrm{i}}}=1+\left(2 \cdot \frac{\mathrm{R}_{\mathrm{F}}}{\mathrm{R}_{\mathrm{G}}}\right)=1+\left(2 \cdot \frac{4.22 \mathrm{k} \Omega}{931 \Omega}\right)=10.06$
The effect of increasing or decreasing the feedback resistor value is shown in Figure 13 on page 12. Increasing $R_{F}$ will tend to roll off the response, while decreasing it will peak the frequency response up, extending the bandwidth. $\mathrm{R}_{\mathrm{G}}$ was adjusted in each of these plots to hold a constant gain of 10 (or 20 dB ). This shows the flexibility offered by the CFA topology-the frequency response can be controlled with the value of the feedback resistor, $\mathrm{R}_{\mathrm{F}}$ ( R 5 and R20), with resistor $\mathrm{R}_{\mathrm{G}}(\mathrm{R} 10)$ setting the desired gain.
The ISL15102 provides two power efficient, high output current CFAs. These are intended to be connected as one differential driver. Power-down control is provided through control pin DIS.

Very low output distortion at low power can be provided by the differential configuration. The high slew rate intrinsic to the CFA topology also contributes to the exceptional performance shown in Figure 16 on page 12. This swept frequency distortion plot shows low distortion at 200 kHz holding to very low levels up through 10 MHz .

### 2.4 Input Biasing and Input Impedance

The ISL15102 has internal resistors at the noninverting inputs for mid-rail biasing, so only external AC coupling capacitors are required for input biasing, shown in Figure 1 on page 3. With two 100 nF coupling capacitors and an input differential impedance of $6 \mathrm{k} \Omega$ typical, the first order high-pass cut-off frequency is 530 Hz .

## 3. PCB Layout Guidelines

For greatest stability, place the feedback resistors $\left(R_{F}\right)$ as close as possible to the output and inverting input pins to minimize parasitic capacitance in the feedback loop. Keep the gain resistor $\left(\mathrm{R}_{\mathrm{G}}\right)$ very close to the inverting inputs for its port and minimize parasitic capacitances to ground or power planes as well.
Close placement of the supply decoupling capacitors will minimize parasitic inductance in the supply path. High frequency load currents are typically pulled through these capacitors, so close placement of $0.01 \mu \mathrm{~F}$ capacitors on each of the supply pins will improve dynamic performance. Higher valued capacitors, $6.8 \mu \mathrm{~F}$ typically, can be placed further from the package because they provide more of the low frequency decoupling.
Connect the thermal pad for the ISL15102 to ground. It is recommended to fill the PCB metal beneath the thermal pad with a $3 \times 3$ array of vias to spread heat away from the package. The larger the PCB metal area, the lower the junction temperature of the device.
Although the ISL15102 is relatively robust in driving parasitic capacitive loads, it is always preferred to place any series output resistors $\left(\mathrm{R}_{\mathrm{S}}\right)$ as close as possible to the output pins. Then trace capacitance on the other side of that resistor will have a much smaller effect on loop phase margin.
Protection devices that are intended to steer large load transients away from the ISL15102 output stage and into the power supplies or ground should have a short trace from their supply connections into the nearest supply capacitor, or they should include their own supply capacitors to provide a low impedance path under fast transient conditions.

### 3.1 ISL15102IRZ-EVAL Schematic



Figure 2. Schematic

### 3.2 ISL15102IRZ-EVALZ Bill of Materials

| Reference Designator | Qty | Manufacturer Part | Assembled | Description | Manufacturer |
| :---: | :---: | :---: | :---: | :---: | :---: |
| C1, C2, C5, C6, C7 | 5 | GRM31C5C1E104JA01L | Yes | CAP CER 0.1UF 25V NP0 1206 | Murata Electronics North America |
| C3, C4, C8, C13, C14 | 5 | C1206C104K5RAC7867 | Yes | CAP CER 0.1UF 50V X7R 1206 | Kemet |
| C17 | 1 | UMK316AB7475KL-T | Yes | CAP CER 0.1UF 50V X7R 1206 | Taiyo Yuden |
| C18 | 1 | None | Yes | Short | None |
| D5 | 1 | UDZVTE-175.1B | Yes | Diode Zener 5.1V 200mW UMD2 | Rohm Semiconductor |
| $\begin{aligned} & \mathrm{J} 1, \mathrm{~J} 3, \mathrm{~J} 4, \mathrm{~J} 5, \mathrm{~J} 6, \mathrm{~J} 7, \\ & \mathrm{~J} 8 \end{aligned}$ | 7 | 112404 | Yes | Conn BNC Jack Str 50 ohm PCB | Amphenol-RF Division |
| J17 | 1 | 6095 | Yes | Jack Non-insulated Recessed Head | Keystone Electronics |
| J18 | 1 | 6095 | Yes | Jack Non-insulated Recessed Head | Keystone Electronics |
| R3, R6, R7,R9, R15, R17, R18, R22, R24 | 9 | CRCW12060000Z0EA | Yes | RES SMD 0.0 OHM JUMPER 1/4W 1206 | Vishay Dale |
| R4, R21 | 1 | CRCW12062R49FKEA | Yes | RES SMD 2.49 OHM 1\% 1/4W 1206 | Vishay Dale |
| R5, R20 | 2 | CRCW12063K01FKEA | Yes | RES SMD 3.01K OHM 1\% 1/4W 1206 | Vishay Dale |
| R8, R23 | 2 | CRCW120649R9FKEA | Yes | RES SMD 49.9 OHM 1\% 1/4W 1206 | Vishay Dale |
| R10 | 1 | CRCW1206619RFKEA | Yes | RES SMD 619 OHM 1\% 1/4W 1206 | Vishay Dale |
| R48 | 1 | CRCW120649R9FKEA | Yes | RES SMD 10K OHM 1\% 1/4W 1206 | Vishay Dale |
| SW1 | 1 | G13AP | Yes | SWITCH TOGGLE SPDT 0.4VA 28 V | NKK |
| TP1, TP2, TP4, TP5, TP6, TP7, TP8, TP9, TP10, TP11, TP12, TP13, TP14, TP15, TP16, TP17, TP18, TP19, TP20, TP21, TP35 | 21 | 1514-2 | Yes | Terminal Turret Double 0.109" L | Keystone |
| U1 | 1 | ISL15102IRZ | Yes |  | Intersil |
| $\begin{aligned} & \text { C9, C10, C12, C15, } \\ & \text { C16 } \end{aligned}$ | 5 | GRM31C5C1E104JA01L | No | CAP CER 0.1UF 25V NP0 1206 | Murata Electronics North America |
| C11 | 1 | C1206C104K5RAC7867 | No | CAP CER 0.1UF 50V X7R 1206 | Kemet |
| D1, D2, D3, D4 | 4 | DDSL01-030SL | No | TVS Diode 30VWM SOT23-3 | STMicroelectronics |
| $\begin{aligned} & \text { J2, J9, J10, J11, J12, } \\ & \text { J13, J14, J15, J16 } \end{aligned}$ | 9 | 112404 | No | Conn BNC Jack Str 50 ohm PCB | Amphenol-RF Division |
| J19 | 1 | 6095 | No | Jack Non-insulated Recessed Head | Keystone Electronics |
| R1, R2, R26, R42, R46, R47 | 6 | CRCW120649R9FKEA | No | RES SMD 49.9 OHM 1\% 1/4W 1206 | Vishay Dale |
| $\begin{aligned} & \mathrm{R} 11, \mathrm{R} 12, \mathrm{R} 25, \mathrm{R} 31, \\ & \mathrm{R} 32, \mathrm{R} 33, \mathrm{R} 38, \mathrm{R} 39, \\ & \mathrm{R} 37, \mathrm{R} 40, \mathrm{R} 45, \mathrm{R} 41 \end{aligned}$ | 10 | CRCW12060000Z0EA | No | RES SMD 0.0 OHM JUMPER 1/4W 1206 | Vishay Dale |
| R27, R44 | 2 | CRCW12062R49FKEA | No | RES SMD 2.49 OHM 1\% 1/4W 1206 | Vishay Dale |
| R13, R19, R28, R34 | 4 | CRCW120649R9FKEA | No | RES SMD 10K OHM 1\% 1/4W 1206 | Vishay Dale |
| R14, R16, R29, R35 | 4 | CRCW12062K00FKEA | No | RES SMD 2K OHM 1\% 1/4W 1206 | Vishay Dale |
| R30, R43 | 2 | CRCW12063K01FKEA | No | RES SMD 3.01K OHM 1\% 1/4W 1206 | Vishay Dale |
| R36 | 1 | CRCW1206619RFKEA | No | RES SMD 619 OHM 1\% 1/4W 1206 | Vishay Dale |
| SW2, SW3, SW4 | 3 | G13AP | No | SWITCH TOGGLE SPDT 0.4VA 28V | NKK |
| T1, T2 | 2 | TT1-6+ | No | RF Transformer 1:150R | Mini-Circuit |


| Reference Designator | Qty | Manufacturer Part | Assembled | Description | Manufacturer |
| :--- | :---: | :---: | :---: | :---: | :---: |
| TP3, TP22, TP23, | 16 | $1514-2$ | No | Terminal Turret Double 0.109" L |  |
| TP24, TP25, TP26, |  |  |  |  |  |
| TP27, TP28, TP29, |  |  |  |  |  |
| TP30, TP31, TP32, |  |  |  |  |  |
| TP33, TP34, TP36, |  |  |  |  |  |
| TP37 |  |  |  |  |  |

### 3.3 ISL15102IRZ-EVAL Board Layout



Figure 3. Top Layer


Figure 5. Ground Layer


Figure 4. Bottom Layer


Figure 6. Power Layer

## 4. Typical Performance Curves

$\mathrm{V}_{\mathrm{S}^{+}}=+12 \mathrm{~V}, \mathrm{R}_{\mathrm{F}}=4.22 \mathrm{k} \Omega, \mathrm{A}_{\mathrm{V}}=10 \mathrm{~V} / \mathrm{V}$ differential, $\mathrm{R}_{\mathrm{L}}=50 \Omega$ differential, $\mathrm{TA}=+25^{\circ} \mathrm{C}, \mathrm{DIS}=0 \mathrm{~V}$


Figure 7. Small Signal Frequency Response vs Gain


Figure 9. 1MHz Harmonic Distortion vs Output Swing


Figure 11. 1MHz Harmonic Distortion vs Load


Figure 8. Large Signal Frequency Response


Figure 10. 4MHz Harmonic Distortion vs Output Swing


Figure 12. 4MHz Harmonic Distortion vs Load
$\mathrm{V}_{\mathrm{S}^{+}}=+12 \mathrm{~V}, \mathrm{R}_{\mathrm{F}}=4.22 \mathrm{k} \Omega, \mathrm{A}_{\mathrm{V}}=10 \mathrm{~V} / \mathrm{V}$ differential, $\mathrm{R}_{\mathrm{L}}=50 \Omega$ differential, $\mathrm{TA}=+25^{\circ} \mathrm{C}, \mathrm{DIS}=0 \mathrm{~V}$ (Continued)


Figure 13. Small Signal Frequency Response vs $\mathbf{R}_{\mathbf{F}}$


Figure 15. Small Signal Frequency Response vs $\mathrm{R}_{\mathrm{S}}$ and $\mathrm{C}_{\text {LOAD }}$


Figure 17. Common-Mode Small Signal Frequency Response vs C Coad


Figure 14. Small Signal Frequency Response vs $C_{\text {LOAD }}$


Figure 16. Harmonic Distortion vs Frequency


Figure 18. Small Signal Frequency Response vs Supply Voltage
$\mathrm{V}_{\mathrm{S}^{+}}=+12 \mathrm{~V}, \mathrm{R}_{\mathrm{F}}=4.22 \mathrm{k} \Omega, \mathrm{A}_{\mathrm{V}}=10 \mathrm{~V} / \mathrm{V}$ differential, $\mathrm{R}_{\mathrm{L}}=50 \Omega$ differential, $\mathrm{TA}=+25^{\circ} \mathrm{C}$, $\mathrm{DIS}=0 \mathrm{~V}$ (Continued)


Figure 19. Package Power Dissipation vs Ambient Temperature

## 5. Revision History

| Rev. | Date |  |
| :---: | :---: | :--- |
| 0.00 | Nov 15, 2017 | Initial release |

ISL15102IRZ-EVALZ

## -ReNESAS

