## High Frequency, Dual Output, Step-Down Supply with EPC GaN FETs

## General Description

Evaluation circuit EVAL-LTC7890-AZ is a dual output synchronous step-down converter that drives all N -channel gallium nitride ( GaN ) field effect transistors (FETs). The EVAL-LTC7890-AZ evaluation board features EPC2218 100V FETs from EPC.

EVAL-LTC7890-AZ features the LTC ${ }^{\circledR 7890}$ : a low quiescent current high frequency (programmable fixed frequency from 100 kHz up to 3 MHz ) dual step-down DC/DC synchronous controller, with a dedicated driver feature for GaN FETs housed in a small $6 \mathrm{~mm} \times 6 \mathrm{~mm}$ QFN package.

The EVAL-LTC7890-AZ operates over an input voltage range from 14 V to 72 V , while the LTC7890 can operate up to 100 V . The EVAL-LTC7890-AZ evaluation circuit produces two outputs: 5 V and 12 V with up to 20 A on each output. EVAL-LTC7890-AZ is configured with sense resistors for current sensing. A mode selector allows the

EVAL-LTC7890-AZ to operate in forced continuous operation, pulse-skipping or Burst Mode ${ }^{\circledR}$ operation during light loads. The EXTVCC pin permits the LTC7890 to be powered from the output of the switching regulator or other available source, reducing power dissipation, and improving efficiency. Refer to the LTC7890 data sheet for a complete description of the part operation and application information.
The performance summary table summarizes the performance of the evaluation circuit at room temperature. The evaluation circuit can be easily modified for different applications, including 2-phase single output. The LTC7890 is housed in a 40-lead ( $6 \mathrm{~mm} \times 6 \mathrm{~mm}$ ), side wettable, QFN package. Refer to the data sheet in conjunction with this EVAL-LTC7890-AZ evaluation circuit user guide.

Design files for this circuit board are available at www.analog.com.

Performance Summary ( $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ )

| PARAMETER | CONDITIONS | MIN | TYP | MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Input Voltage Range | Maximum Component Temperature $<100^{\circ} \mathrm{C}$, l $_{\text {OUT1 }}=$ l $_{\text {OUT2 }}=20 \mathrm{~A}$, With Heatsink and 400LFM Airflow, After 10-minute run time | 14 |  | 72 | V |
|  | Maximum Component Temperature = $100^{\circ} \mathrm{C}, \mathrm{I}_{\text {OUT1 }}=\mathrm{I}_{\text {OUT2 }}=20 \mathrm{~A}$, With Heatsink, No Airflow, After 10-minute run time | 14 |  | 52 | V |
|  | Maximum Component Temperature = $100^{\circ} \mathrm{C}$, I IUUT1 $=$ I OUT2 $=20 \mathrm{~A}$, No Heatsink, No Airflow, After 10-minute run time | 14 |  | 32 | V |
|  | $\text { IOUT1 }=\text { IOUT2 }=20 \mathrm{~A},$ <br> <1 minute run time maximum | 14 |  | 72 | V |
| Output Voltage, $\mathrm{V}_{\text {OUT1 }}$ | $\mathrm{V}_{\text {IN }}=14 \mathrm{~V}-72 \mathrm{~V}, \mathrm{VPRG} 1=0 \mathrm{~V}$ | 4.925 | 5 | 5.075 | V |
| Output Voltage Ripple, $\mathrm{V}_{\text {OUT1 }}(\mathrm{AC})$ | $\mathrm{V}_{\text {IN }}=48 \mathrm{~V}, \mathrm{I}_{\text {OUT }}=20 \mathrm{~A}$ |  | 40 |  | $\mathrm{mV} \mathrm{P}_{\text {-P }}$ |
| Output Voltage, $\mathrm{V}_{\text {OUT2 }}$ | $\mathrm{V}_{\text {IN }}=14 \mathrm{~V}-72 \mathrm{~V}$ | 11.76 | 12 | 12.24 | V |
| Output Voltage Ripple, V ${ }_{\text {OUT2(AC) }}$ | $\mathrm{V}_{\text {IN }}=48 \mathrm{~V}$, $\mathrm{I}_{\text {OUT }}=20 \mathrm{~A}$ |  | 80 |  | $\mathrm{mV} \mathrm{P}_{\text {- }}$ |
| Input Current | $\mathrm{FCM}, \mathrm{V}_{\text {IN }}=48 \mathrm{~V}, \mathrm{I}_{\text {OUT1 }}=\mathrm{I}_{\text {OUT2 }}=0 \mathrm{~A}$ |  | 48.9 |  | mA |
|  | Burst Mode, $\mathrm{V}_{\text {IN }}=48 \mathrm{~V}, \mathrm{I}_{\text {OUT1 }}=\mathrm{I}_{\text {OUT2 }}=0 \mathrm{~A}$ |  | 10 |  | $\mu \mathrm{A}$ |
| Typical Switching Frequency | P3 = DISABLE SS (SSFM OFF) |  | 500 |  | kHz |
|  | P3 = ENABLE SS (SSFM ON) | 500 |  | 600 | kHz |
| Efficiency | $\mathrm{V}_{\text {IN }}=48 \mathrm{~V}, \mathrm{~V}_{\text {OUT1 }}=5 \mathrm{~V}$, $\mathrm{I}_{\text {OUT } 1}=20 \mathrm{~A}$ |  | 94.0 |  | \% |
|  | $\mathrm{V}_{\text {IN }}=48 \mathrm{~V}, \mathrm{~V}_{\text {OUT2 }}=12 \mathrm{~V}, \mathrm{I}_{\text {OUT2 }}=20 \mathrm{~A}$ |  | 96.9 |  | \% |

## Quick Start Procedure

The EVAL-LTC7890-AZ evaluation circuit is easy to set up to evaluate the performance of the LTC7890. See Figure 1 for proper measurement equipment setup and follow the procedure below:

1. With power off, connect the input power supply to $V_{I N}$ and GND.
2. Connect the output loads between Vout1 and GND, and Vout2 and GND.
3. Turn on the power at the input. Increase Vin slowly to 14 V . Make sure RUN1 and RUN2 switches are on the ON position.

NOTE: Make sure that the input voltage is always within the specified range.
4. Check for the proper output voltages. The output should be regulated at 5 V for Channel 1 and 12 V for channel 2.
5. Once the proper output voltage is established, adjust the input voltage and load current within the operating range and observe the output voltage regulation, ripple voltage, efficiency, and other parameters.

NOTE: When measuring the input or output voltage ripples, take care to avoid a long ground lead on the oscilloscope probe. Measure the input or output voltage ripple by touching the probe tip directly across the Vin or Vout and GND terminals or directly across the relevant capacitor. See Figure 2 for the proper probe technique.

## Adjusting the Output Voltage

The LTC7890 includes an output voltage control pin for Channel 1 VPRG1. This pin allows for the output voltage of Channel 1 to be set to a fixed $12 \mathrm{~V}, 5 \mathrm{~V}$ or an external feedback resistor divider can be used to set the output voltage from 0.8 V to 60 V . EVAL-LTC7890-AZ has the Channel 1 output voltage set to 5 V by connecting VPRG1 to GND and connecting VFB1 to $\mathrm{V}_{\text {OUT1 }}$ through R18. To change the output voltage from the programmed 5 V , float the VPRG1 pin by removing R43 and change R18 and R19. Refer to the Setting the Output Voltage section on the data sheet for calculating the $\mathrm{V}_{\mathrm{FB}}$ resistor divider values for the desired output voltage. All the corresponding power components will also need to be changed to meet the desired output voltage.
For Channel 2 of the LTC7890, the output voltage can be set from a range of 0.8 V to 60 V using a feedback resistor divider. To change the output voltage from the programmed 12 V , change R23 and R32. Refer to the Setting the Output Voltage section on the data sheet for calculating the $V_{\text {FB2 }}$ resistor divider values for the desired output voltage. All the corresponding power components will also need to be changed to meet the desired output voltage.

## Setting the Switching Frequency

Selecting the switching frequency is a trade-off between efficiency and component size. For optimal performance, a switching frequency of 500 kHz is chosen. R37 programs the desired switching frequency. The switching frequency is set using FREQ and PLLIN/SPREAD pins. Refer to the Setting the Operating Frequency section in the LTC7890 data sheet for details.

## RUN Control (RUN1, S1, RUN2, S2)

The RUN1 and RUN2 turrets of the evaluation circuit serve as an external on/off control for Channel 1 and Channel 2, respectively. The EVAL-LTC7890-AZ includes a resistive voltage divider for each channel connected between $\mathrm{V}_{\text {IN }}$ and GND to turn on the device at the required input voltage. Turn switch 1 (S1) to the ON position to connect the RUN1 pin to the center of this resistor divider for Channel 1, and turn switch 2 (S2) to the ON position to connect the RUN2 pin to the center of this resistor divider for Channel 2. The EVAL-LTC7890-AZ connects the run pin of both channels to the $\mathrm{V}_{\mathrm{IN}}$ for always-on operation. Both channels will begin switching once the input voltage rises above the INTVCC UVLO threshold off 3.8 V . A desired threshold can be easily added by changing the resistor divider on each channel. See Table 3 to configure S1 and Table 4 to configure S2.

## TRACK and Soft-Start Inputs (TRACK/SS)

LTC7890's TRACK/SS1 and TRACK/SS2 pins can be used to program an external soft-start function or to allow Vout to track another supply during startup for Channel 1 and Channel 2, respectively. The adjustable soft-start function is used to limit the inrush current during startup. The soft-start time is adjusted by C17. An external supply can be connected to the TRK/SS turrets to make the startup of the VOUT track an external supply. Typically, this requires connecting to the TRK/SS turret through an external resistor divider from the external supply to GND. Refer to the Soft-Start and Tracking section on the data sheet.

## Mode Selection (MODE, P1)

EVAL-LTC7890-AZ provides a jumper (P1) to allow the LTC7890 to operate in either Forced Continuous, Pulse Skipping, or Burst modes at lighter loads. Refer to the LTC7890 data sheet for more details on the modes of operation. Table 1 shows the mode selection P1 settings that can be used to configure the desired mode of operation.

## Spread Spectrum, Phase-Locked Loop and External Frequency Synchronization (PLLIN/SPREAD, P3)

The LTC7890 features spread spectrum mode operation to improve EMI. This mode varies the switching frequency within the typical boundaries of the frequency set by the FREQ pin and $+20 \%$. Spread spectrum operation is enabled by tying the PLLIN/SPREAD pin to INTV ${ }_{C C}$. EVAL-LTC7890-AZ includes a jumper (P3) to conveniently enable or disable the spread spectrum operation. See Table 2 to configure P3.

The LTC7890 also features a phase-locked loop to synchronize the internal oscillator to an external clock source. EVAL-LTC7890-AZ provides a SYNC turret to connect the external clock source to synchronize with the device switching. Keep the jumper (P3) in the external sync position when the external clock signal is applied. Refer to the LTC7890 data sheet for more details about external clock synchronization.

## Open-Drain PGOOD Outputs (PGOOD)

EVAL-LTC7890-AZ provides PGOOD1 and PGOOD2 turrets to monitor the status of the PGOOD output for Channel 1 and Channel 2, respectively. PGOOD is high when the $\mathrm{V}_{\mathrm{FB}}$ voltage is within $\pm 10 \%$ of the 0.8 V reference. PGOOD is pulled low when the $V_{F B}$ voltage is not within $0.8 \mathrm{~V} \pm 10 \%$ or the RUN pin is low (shutdown). The voltage on the PGOOD pins should not exceed 6V.

## EXTV $_{\text {Cc }}$ Linear Regulator

The EXTV ${ }_{C C}$ pin allows the $I N T V_{C C}$ power to be derived from a high efficiency external source. On EVAL-LTC7890-AZ, the EXTV ${ }_{C C}$ pin is connected to $V_{\text {OUT1 }}$. The EXTV ${ }_{C C}$ turret can be used to connect an external power supply to source the EXTV ${ }_{C C}$ LDO. When using an external power supply on the EXTV ${ }_{C C}$ turret, make sure to disconnect the $V_{\text {OUT }}$ connection to the EXTV ${ }_{C C}$ pin by removing R59. Populate $R 61$ with a $0 \Omega$ resistor.

## 2-Phase Single Output Operation

The two channels of the LTC7890 can be operated in a 2-phase single output configuration for high-current applications. EVAL-LTC7890-AZ includes all the necessary component place holders to configure the board to 2-phase single output operation. Refer to the 2-Phase Single Output Operation section of the LTC7890 data sheet for the required modifications.

## Thermal Performance

The EVAL-LTC7890-AZ features excellent thermal performance due to the high efficiency of the synchronous step-down GaN FET controller circuitry. The component temperatures of EVAL-LTC7890-AZ with a 32V input and 20A load on both channels at the same time are shown in Figure 13. The capture was taken after 10 minutes of operation. For short pulses, the board can perform at the maximum power rating for the entire input voltage range. The six-layer PCB layout features solid copper planes that provide adequate heat spreading across the whole board.

With an input voltage higher than 32 V , the circuit needs a heatsink and/or forced air flow to keep the maximum temperature of the board under $100^{\circ} \mathrm{C}$ to achieve full power and run for more than 10 minutes. With a heatsink, the board can operate with a 20 A load on both channels at the same time, up to an input voltage of 52 V . With a heatsink and 400 LFM of airflow, the board can operate at the full input voltage range of 14 V to 72 V with a 20 A load on both channels at the same time. See Figure 11 for the recommended maximum load current on each channel.

## Heatsink

The EVAL-LTC7890-AZ features space for a heatsink to extend the power and thermal capabilities significantly. The board is designed for the Wakefield-Vette 567-45AB heatsink and is to be used in conjunction with thermal pads and Wurth Elektronik 9774010243 R spacers. The spacers should be soldered onto P10, P11, P12, and P13, and a thermal pad placed between the heatsink and the GaN FETs. Properly screw in the heatsink to fully extend the power capabilities of the board.


Figure 1. EVAL-LTC7890-AZ Board Connections


Figure 2. EVAL-LTC7890-AZ Ripple Measurement

## Table 1. MODE Selection Jumper (P1) Settings

| SHUNT POSITION | MODE PIN | MODE |
| :---: | :---: | :---: |
| $1-2^{*}$ | Connected to INTV CC | FCM mode of operation |
| $3-4$ | Connected to INTV $\mathrm{CC}_{\mathrm{C}}$ with a $100 \mathrm{k} \Omega$ | Pulse-Skipping mode of operation |
| $5-6$ | Connected to GND | Bust mode of operation |

*Default position
Table 2. PLLIN/SPREAD Jumper (P3) Settings

| SHUNT POSITION | PLLIN/SPREAD PIN | DESCRIPTION |
| :---: | :---: | :---: |
| $1-2$ | Connected to INTV ${ }_{\mathrm{CC}}$ | Enable SS |
| $3-4^{*}$ | Connected to GND | Disable SS |
| $5-6$ | Connected to the center node of R49 and C16 | External SYNC input |

*Default position

Table 3. RUN1 Switch (S1) Settings

| SWITCH POSITION | RUN PIN | CONTROLLER |
| :---: | :---: | :---: |
| ON | Connected to $\mathrm{V}_{\text {IN }}$ | Set to startup Channel 1 when $\mathrm{V}_{\text {IN }}$ is <br> applied |
| OFF* $^{\text {Connected to GND }}$ | Disabled |  |

*Default position

Table 4. RUN2 Switch (S2) Settings

| SWITCH POSITION | RUN PIN | CONTROLLER |
| :---: | :---: | :---: |
| ON | Connected to $\mathrm{V}_{\text {IN }}$ | Set to startup Channel 2 when $\mathrm{V}_{I N}$ is <br> applied |
| OFF* | Connected to GND | Disabled |

*Default position

## Performance

( $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$, unless otherwise noted.)


$$
V_{\text {out } 1}=5 \mathrm{~V}, \mathrm{f}_{\mathrm{sw}}=500 \mathrm{kHz} \text {, FCM Mode }
$$

Figure 3. Channel 1 Efficiency vs. Load Current

$\mathrm{V}_{\mathrm{IN}}=48 \mathrm{~V}, \mathrm{~V}_{\text {OUT } 1}=5 \mathrm{~V}, \mathrm{f}_{\mathrm{sw}}=500 \mathrm{kHz}$
Figure 5. Channel 1, Efficiency and Power Loss vs. Load Current

$\mathrm{V}_{\text {IN }}=48 \mathrm{~V}, \mathrm{~V}_{\text {OUT } 1}=5 \mathrm{~V}$, Iout $1=20 \mathrm{~A}(20 \mathrm{MHz} \mathrm{BW})$
Figure 7. Channel 1 Output Voltage Ripple

$\mathrm{V}_{\text {IN }}=48 \mathrm{~V}, \mathrm{~V}_{\text {out } 1}=5 \mathrm{~V}$, lout $=10 \mathrm{~A}-20 \mathrm{~A}-10 \mathrm{~A}$
Figure 9. Channel 1 Load Transient Response

$\mathrm{V}_{\text {out } 2}=12 \mathrm{~V}, \mathrm{f}_{\mathrm{sw}}=500 \mathrm{kHz}$, FCM Mode
Figure 4. Channel 2 Efficiency vs. Load Current


$$
\mathrm{V}_{\mathrm{IN}}=48 \mathrm{~V}, \mathrm{~V}_{\mathrm{OUT} 2}=12 \mathrm{~V}, \mathrm{f}_{\mathrm{sw}}=500 \mathrm{kHz}
$$

Figure 6. Channel 2, Efficiency and Power Loss vs. Load Current

$\mathrm{V}_{\text {IN }}=48 \mathrm{~V}, \mathrm{~V}_{\text {OUT } 2}=12 \mathrm{~V}$, lout $2=20 \mathrm{~A}(20 \mathrm{MHz} \mathrm{BW})$
Figure 8. Channel 2 Output Voltage Ripple

$\mathrm{V}_{\text {IN }}=48 \mathrm{~V}, \mathrm{~V}_{\text {OUT2 }}=12 \mathrm{~V}$, lout $2=10 \mathrm{~A}-20 \mathrm{~A}-10 \mathrm{~A}$
Figure 10. Channel 2 Load Transient Response


Figure 11. Maximum recommended output current vs. $V_{I N}$ with the same load current on both channels while simultaneously keeping the maximum board temperature under $100^{\circ} \mathrm{C}$ after running for 10 minutes. With a heatsink, the board can operate at maximum load on both channels simultaneously from an input of 14 V to 52 V . With a Heatsink and airflow, the board can operate at the maximum load current for the full input voltage range.

$\mathrm{V}_{\text {IN }}=48 \mathrm{~V}, \mathrm{~V}_{\text {OUT } 1}=5 \mathrm{~V}$, I Iout $1=20 \mathrm{~A}, \mathrm{~V}_{\text {OUT2 }}=12 \mathrm{~V}$, I Iott $=20 \mathrm{~A}$
With Heatsink, No Airflow
Figure 12. Full power can be achieved on both channels simultaneously with the addition of the heatsink.

$\mathrm{V}_{\text {IN }}=32 \mathrm{~V}, \mathrm{~V}_{\text {OUT } 1}=5 \mathrm{~V}, \mathrm{I}_{\text {OUT } 1}=20 \mathrm{~A}, \mathrm{~V}_{\text {OUT } 2}=12 \mathrm{~V}, \mathrm{I}_{\text {OUT } 2}=20 \mathrm{~A}$ No Heatsink, No Airflow
Figure 13. Without the heatsink, the component temperature can rise to $100^{\circ} \mathrm{C}$ after running for 10 minutes at $32 V_{I N}$.

## Bill of Materials

| ITEM | QTY | DESIGNATOR | DESCRIPTION | MANUFACTURER PART NUMBER |
| :---: | :---: | :---: | :---: | :---: |
| REQUIRED CIRCUIT COMPONENTS |  |  |  |  |
| 1 | 1 | C1 | CAP. 4.7 $\mu \mathrm{F}, \mathrm{X} 5 \mathrm{R}, 25 \mathrm{~V}, 10 \%, 0603$, AEC-Q200 | MURATA, GRM188R61E475KE13D |
| 2 | 1 | C11 | CAP., 100pF, X8R, 50V, 10\%, 0603 | TDK, C1608X8R1H101K |
| 3 | 1 | C12 | CAP., 3300pF, X7R, 50V, 10\%, 0603 | YAGEO, CC0603KRX7R9BB332 |
| 4 | 1 | C14 | CAP., 6800pF, X7R, 50V, 10\%, 0603 | YAGEO, CC0603KRX7R9BB682 |
| 5 | 5 | C2, C3, C4, C15, C17 | CAP., 0.1 $\mu \mathrm{F}, \mathrm{X7R}, 25 \mathrm{~V}, 10 \%$, 0603 | KEMET, C0603C104K3RACTU |
| 6 | 2 | C20, C24 | CAP., 100pF, X7R, 50V, 10\%, 0603 | KEMET, C0603C101K5RAC |
| 7 | 1 | C23 | CAP., 1 1 F, X7R, 25V, 10\%, 0603, AEC-Q200 | MURATA, GCM188R71E105KA64D |
| 8 | 1 | C25, C27 | CAP., $0.1 \mu \mathrm{~F}, \mathrm{X7R}, 100 \mathrm{~V}, 10 \%$, 0603 | MURATA, GRM188R72A104KA35D |
| 9 | 13 | $\begin{aligned} & \mathrm{C} 26, \mathrm{C} 28, \mathrm{C} 29, \mathrm{C} 30, \mathrm{C} 31, \\ & \mathrm{C} 32, \mathrm{C} 33, \mathrm{C} 34, \mathrm{C} 35, \mathrm{C} 36, \\ & \mathrm{C} 37, \mathrm{C} 38, \mathrm{C} 39 \end{aligned}$ | $\begin{aligned} & \text { CAP., } 0.22 \mu \mathrm{~F}, \mathrm{X} 7 \mathrm{~S}, 100 \mathrm{~V}, 10 \%, 0603, \text { AEC- } \\ & \text { Q200 } \end{aligned}$ | TAIYO YUDEN, HMK107C7224KAHTE |
| 10 | 2 | C5, C7 | CAP., 1000pF, X7R, 25V, 10\%, 0603 | AVX, 06033C102KAT2A |
| 11 | 2 | CIN1, CIN2 | CAP., $56 \mu \mathrm{~F}, \mathrm{AL}-\mathrm{POLY}, 80 \mathrm{~V}, 20 \%$ | PANASONIC, 80SXV56M |
| 12 | 6 | CIN9, CIN10, CIN11, CIN16, CIN17, CIN18 | CAP., 1 1 F, X7S, 100V, 10\%, 0805 | TDK, C2012X7S2A105K125AB |
| 13 | 8 | COUT1, COUT2, COUT5, COUT6, COUT11, COUT12, COUT14, COUT18 | CAP., 22 $\mu \mathrm{F}, \mathrm{X7R}, 16 \mathrm{~V}, 10 \%$, 1210 | MURATA, GRM32ER71C226KEA8L |
| 14 | 1 | COUT4, COUT8, COUT10, COUT15 | CAP., 150 ${ }^{\text {F }}$, TANT., 16V, 20\%, 7343 | PANASONIC, 16TQC150MYF |
| 15 | 2 | L1, L2 | IND., $2 \mu \mathrm{H}, \mathrm{PWR}, 20 \%, 40 \mathrm{~A}, 1.34 \mathrm{~m} \Omega$ 18.7X19.18mm, AEC-Q200 | COILCRAFT, SER2011-202MLD |
| 16 | 4 | Q1, Q2, Q3, Q4 | XSTR., PWR, GaNFET, 100V, 60A/231A, DIE SIZE: $3.5 \times 1.95 \mathrm{~mm}$ | EFFICIENT POWER CONVERSION, EPC2218 |
| 17 | 12 | $\begin{aligned} & \text { R2, R3, R18, R25, R28, } \\ & \text { R36, R41, R43, R48, R50, } \\ & \text { R52, R59 } \end{aligned}$ | RES., 0 ${ }^{\text {, 1/10W,0603, AEC-Q200 }}$ | VISHAY, CRCW06030000Z0EA |
| 18 | 2 | R1, R5 | RES., 1M 2 , 1\%, 1/10W, 0603, AEC-Q200 | VISHAY, CRCW06031M00JNEA |
| 19 | 1 | R12 | RES., 10ת, 1\%, 1/10W, 0603, AEC-Q200 | VISHAY, CRCW060310ROFKEA |
| 20 | 6 | $\begin{aligned} & \text { R8, R9, R13, R14, R15, } \\ & \text { R16 } \end{aligned}$ | RES., 1ת, 5\%, 1/16W, 0402, AEC-Q200 | VISHAY, CRCW04021R00JNED |
| 21 | 2 | R17, R24 | RES., 10ת, 1\%, 1/10W, 0603, AEC-Q200 | PANASONIC, ERJ-3EKF10R0V |
| 22 | 1 | R20 | RES., 3.01k , 1\%, 1/10W, 0603 | TE CONNECTIVITY, CPF0603B3K01E1 |
| 23 | 1 | R21 | RES., $5.9 \mathrm{k} \Omega$, 1\%, 1/10W, 0603, AEC-Q200 | PANASONIC, ERJ-3EKF5901V |
| 24 | 1 | R23 | RES., 1.4M ${ }^{\text {, 1\%, 1/10W, 0603, AEC-Q200 }}$ | VISHAY, CRCW06031M40FKEA |
| 25 | 1 | R29 | RES., 20ת, 1\%, 1/10W, 0603, AEC-Q200 | VISHAY, CRCW060320R0FKEA |
| 26 | 1 | R32 | RES., 100k $\Omega$, 1\%, 1/10W, 0603 | VISHAY, CRCW0603100KFKEA |
| 27 | 1 | R37 | RES., 75k $\Omega$, 1\%, 1/10W, 0603, AEC-Q200 | PANASONIC, ERJ-3EKF7502V |
| 28 | 1 | R49 | RES., 1k $2,1 \%, 1 / 10 \mathrm{~W}, 0603$, AEC-Q200 | PANASONIC, ERJ-3EKF1001V |
| 29 | 2 | R56, R62 | RES., 1M 2 , 1\%, 1/10W, 0603, AEC-Q200 | PANASONIC, ERJ-2RKF1004X |
| 30 | 1 | R57 | RES., 100k , 1\%, 1/10W, 0603, AEC-Q200 | PANASONIC, ERJ-3EKF1003V |

analog.com

| Rev. 0 | 8 of 12 |
| :--- | :--- |


| 31 | 1 | R6 | RES., 1.2 $2,5 \%, 1 / 16 \mathrm{~W}, 0402$, AEC-Q200 | VISHAY, CRCW04021R20FKED |
| :---: | :---: | :---: | :---: | :---: |
| 32 | 1 | R7 | RES., 2.2ת, 5\%, 1/16W, 0402, AEC-Q200 | VISHAY, CRCW04022R20JNED |
| 33 | 2 | RS1, RS2 | RES., 0.0015 ${ }^{\text {, }} 1 \%$, 3W, 2512, AEC-Q200 | VISHAY, WSLP25121L500FEA |
| 34 | 2 | S1, S2 | SWITCH SLIDE DPDT 300MA 6V Through Hole | C\&K, JS202011CQN |
| 35 | 1 | U1 | IC, Dual Step-Down Controller for GaN FETs, side wettable plastic QFN-40 | ANALOG DEVICES, LTC7890RUJM\#PBF |
| OPTIONAL CIRCUIT COMPONENTS |  |  |  |  |
| 1 | 0 | C10 | CAP., 100pF, X7R, 50V, 10\%, 0603 | KEMET, C0603C101K5RAC |
| 2 | 0 | C6, C8, C9, C13, C16 | CAP., OPTION, 0603 |  |
| 3 | 0 | CIN7, CIN8, CIN12, CIN13, CIN15, CIN19, CIN20 | CAP., 1رF, X7S, 100V, 10\%, 0805 | TDK, C2012X7S2A105K125AB |
| 4 | 0 | CIN3, CIN4, CIN5, CIN6 | CAP., 22 FF, X7S, 100V, 20\%, 2 Stacked | TDK, CKG57NX7S2A226M500JH |
| 5 | 0 | COUT3, COUT7, COUT9, COUT13 | CAP., 150رF, TANT., 16V,20\%, 7343 | PANASONIC, 16TQC150MYF |
| 6 | 0 | D1, D2 | DIODE, SCHOTTKY, 100V, 10A, TO-277A, AECQ101 | VISHAY, SS10PH10-M3/86A |
| 7 | 0 | J10, J11 | CONN., RF/COAX, MMCX, JACK, FEMALE, VERT, ST, SMT | MOLEX, 73415-2063 |
| 8 | 0 | R10, R39 | RES., OPTION, 0402 |  |
| 9 | 0 | $\begin{aligned} & \text { R19, R22, R26, R27, R30, } \\ & \text { R31, R33, R34, R38, R40, } \\ & \text { R42, R45, R46, R47, R51, } \\ & \text { R53, R58, R60, R61, R63, } \\ & \text { R66, R68, R71, R72, R74 } \\ & \hline \end{aligned}$ | RES., OPTION, 0603 |  |
| 10 | 0 | R67 | RES., OPTION, 2512 |  |
| 11 | 0 |  | THERMAL INTERFACE MATERIAL | T-GLOBAL, TG-A1780 X 0.5mm |
| 12 | 0 | MP5 | HEATSINK 1/8 BRICK 55X20.7X11.4M | WAKEFIELD-VETTE, 567-45AB |
|  |  |  |  |  |
| HARDWARE - FOR EVALUTATION CIRCUIT ONLY |  |  |  |  |
| 1 | 15 | E1, E2, E3, E4, E5, E6, E7, E8, E9, E10, E11, E12, E13, E16, E17 | TEST POINT, TURRET, 0.094" MTG. HOLE, PCB 0.062" THICK | $\begin{aligned} & \text { MILL-MAX, } \\ & \text { 2501-2-00-80-00-00-07-0 } \end{aligned}$ |
| 2 | 6 | J1, J2, J3, J4, J5, J6 | THREADED BROACHING STUD, 625MIL LENGTH | PENN ENGINEERING, KFH- 032-10ET |
| 3 | 2 | P1, P3 | CONN., HDR, MALE, $2 \times 3,2 \mathrm{~mm}$, VERT, STR, THT | WURTH ELEKTRONIK, 62000621121 |
| 4 | 4 | MP1, MP2, MP3, MP4 | STANDOFF, NYLON, SNAP-ON, 0.625 (5/8"), 15.9 mm | KEYSTONE, 8834 |
| 5 | 2 | XP1, XP3 | CONN., SHUNT, FEMALE, 2 POS, 2 mm | WURTH ELEKTRONIK, 60800213421 |
| 6 | 4 | P10, P11, P12, P13 | CONN-PCB 1POS STEEL SPACER WITH M2X0.4 THD | WURTH ELEKTRONIK, 9774010243R |
|  |  |  |  |  |

## Schematic



## Revision History

| Revision Number | Revision Date | Nature of Change | Page Number |
| :---: | :---: | :---: | :---: |
| Rev 0 | $12 / 23$ | Initial Release | - |

ASSUMED BY ANALOG DEVICES FOR ITS USE, NOR FOR ANY INFRINGEMENTS OF PATENTS OR OTHER RIGHTS OF THIRD PARTIES THAT MAY RESULT FROM ITS USE. SPECIFICATIONS ARE SUBJECT TO CHANGE WITHOUT NOTICE. NO LICENCE, EITHER EXPRESSED OR IMPLIED, IS GRANTED UNDER ANY ADI PATENT RIGHT, COPYRIGHT, MASK WORK RIGHT, OR ANY OTHER ADI INTELLECTUAL PROPERTY RIGHT RELATING TO ANY COMBINATION, MACHINE, OR PROCESS WHICH ADI PRODUCTS ALL INFORMATION CONTAINED HEREIN IS PROVIDED "AS IS" WITHOUT REPRESENTATION OR WARRANTY. NO RESPONSIBILITY IS OR SERVICES ARE USED. TRADEMARKS AND REGISTERED TRADEMARKS ARE THE PROPERTY OF THEIR RESPECTIVE OWNERS.

