

1.1A, 35MHz Current Feedback Amplifier

FEATURES

- 1.1A Minimum Output Drive Current
- 35MHz Bandwidth, $A_V = 2$, $R_I = 10\Omega$
- 900V/ μ s Slew Rate, $A_V = 2$, $R_I = 10\Omega$
- High Input Impedance: 10MΩ
- Wide Supply Range: ±5V to ±15V (TO-220 and DD Packages)
- Enhanced θ_{JA} SO-16 Package for ±5V Operation
- Shutdown Mode: I_S < 200μA
- Adjustable Supply Current
- Stable with $C_1 = 10,000pF$
- Available in 7-Lead DD, TO-220 and 16-Lead SO Packages

APPLICATIONS

- Cable Drivers
- Buffers
- Test Equipment Amplifiers
- Video Amplifiers
- ADSL Drivers

DESCRIPTION

The LT®1210 is a current feedback amplifier with high output current and excellent large-signal characteristics. The combination of high slew rate, 1.1A output drive and ±15V operation enables the device to deliver significant power at frequencies in the 1MHz to 2MHz range. Short-circuit protection and thermal shutdown ensure the device's ruggedness. The LT1210 is stable with large capacitive loads, and can easily supply the large currents required by the capacitive loading. A shutdown feature switches the device into a high impedance and low supply current mode, reducing dissipation when the device is not in use. For lower bandwidth applications, the supply current can be reduced with a single external resistor.

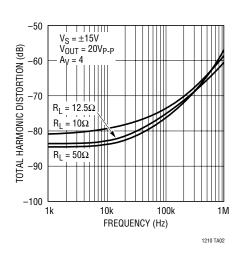
The LT1210 is available in the TO-220 and DD packages for operation with supplies up to ± 15 V. For ± 5 V applications the device is also available in a low thermal resistance SO-16 package.

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TYPICAL APPLICATION

Twisted Pair Driver $\begin{array}{c} 15V \\ \hline \\ 4.7\mu F^* \\ \hline \\ -15V \\ \hline \\ \end{array} \begin{array}{c} R_T \\ 11\Omega \\ 2.5W \\ \hline \\ \end{array} \begin{array}{c} R_T \\ 11\Omega \\ 2.5W \\ \hline \\ \end{array}$

Total Harmonic Distortion vs Frequency



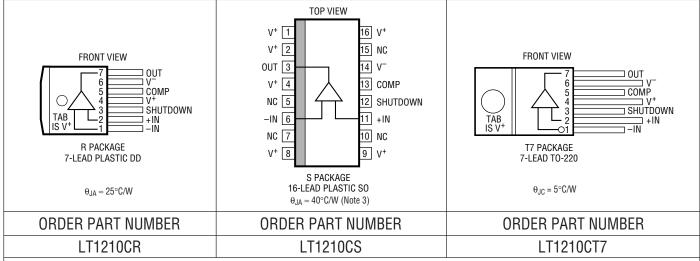


ABSOLUTE MAXIMUM RATINGS (Note 1)

Supply Voltage	±18V
Input Current	±15mA
Output Short-Circuit Duration (Note 2)	Continuous
Specified Temperature Range (Note 3)	0°C to 70°C

Operating Temperature Range40°C t	o 85°C
Junction Temperature	150°C
Storage Temperature Range65°C to	150°C
Lead Temperature (Soldering, 10 sec)	300°C

PACKAGE/ORDER INFORMATION



Order Options Tape and Reel: Add #TR

Lead Free: Add #PBF Lead Free Tape and Reel: Add #TRPBF Lead Free Part Marking: http://www.linear.com/leadfree/

Consult LTC Marketing for parts specified with wider operating temperature ranges.

ELECTRICAL CHARACTERISTICS The ullet denotes specifications which apply over the full operating temperature range, otherwise specifications are at $T_A = 25^{\circ}C$. $V_{CM} = 0V$, $\pm 5V \le V_S \le \pm 15V$, pulse tested, $V_{SD} = 0V$, unless otherwise noted.

SYMBOL	PARAMETER	CONDITIONS		MIN	TYP	MAX	UNITS
V _{OS}	Input Offset Voltage	T _A = 25°C	•		±3	±15 ±20	mV mV
	Input Offset Voltage Drift		•		10		μV/°C
I _{IN} +	Noninverting Input Current	T _A = 25°C	•		±2	±5 ±20	μA μA
I _{IN} ⁻	Inverting Input Current	T _A = 25°C	•		±10	±60 ±100	μΑ μΑ
e _n	Input Noise Voltage Density	$f = 10kHz$, $R_F = 1k$, $R_G = 10\Omega$, $R_S = 0\Omega$			3.0		nV/√Hz
+i _n	Input Noise Current Density	$f = 10kHz, R_F = 1k, R_G = 10\Omega, R_S = 10k$			2.0		pA/√Hz
-i _n	Input Noise Current Density	$f = 10kHz, R_F = 1k, R_G = 10\Omega, R_S = 10k$			40		pA/√Hz
R _{IN}	Input Resistance	$V_{IN} = \pm 12V, V_S = \pm 15V$ $V_{IN} = \pm 2V, V_S = \pm 5V$	•	1.50 0.25	10 5		MΩ MΩ
C _{IN}	Input Capacitance	$V_S = \pm 15V$			2		pF
	Input Voltage Range	$V_S = \pm 15V$ $V_S = \pm 5V$	•	±12 ±2	±13.5 ±3.5		V
							1210fa

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ELECTRICAL CHARACTERISTICS The ullet denotes specifications which apply over the full operating temperature range, otherwise specifications are at $T_A = 25^{\circ}C$. $V_{CM} = 0V$, $\pm 5V \le V_S \le \pm 15V$, pulse tested, $V_{SD} = 0V$, unless otherwise noted.

SYMBOL	PARAMETER	CONDITIONS		MIN	TYP	MAX	UNITS
CMRR	Common Mode Rejection Ratio	$V_S = \pm 15V, V_{CM} = \pm 12V$ $V_S = \pm 5V, V_{CM} = \pm 2V$	•	55 50	62 60		dB dB
	Inverting Input Current Common Mode Rejection	$V_S = \pm 15V, V_{CM} = \pm 12V$ $V_S = \pm 5V, V_{CM} = \pm 2V$	•		0.1 0.1	10 10	μΑ/V μΑ/V
PSRR	Power Supply Rejection Ratio	$V_S = \pm 5V$ to $\pm 15V$	•	60	77		dB
	Noninverting Input Current Power Supply Rejection	$V_S = \pm 5V \text{ to } \pm 15V$	•		30	500	nA/V
	Inverting Input Current Power Supply Rejection	$V_S = \pm 5V \text{ to } \pm 15V$	•		0.7	5	μA/V
A _V	Large-Signal Voltage Gain	$ \begin{array}{l} T_A = 25^{\circ}\text{C}, \ V_S = \pm 15\text{V}, \ V_{OUT} = \pm 10\text{V}, \\ R_L = 10\Omega \ (\text{Note 3}) \end{array} $		55	71		dB
		$V_S = \pm 15V$, $V_{OUT} = \pm 8.5V$, $R_L = 10\Omega$ (Note 3)	•	55	68		dB
		$V_S = \pm 5V$, $V_{OUT} = \pm 2V$, $R_L = 10\Omega$	•	55	68		dB
R_{OL}	Transresistance, $\Delta V_{OUT}/\Delta I_{IN}^-$	$ \begin{array}{l} T_A = 25^{\circ}\text{C}, \ V_S = \pm 15\text{V}, \ V_{OUT} = \pm 10\text{V}, \\ R_L = 10\Omega \ (\text{Note 3}) \end{array} $		100	260		kΩ
		$V_S = \pm 15V$, $V_{OUT} = \pm 8.5V$, $R_L = 10\Omega$ (Note 3)	•	75	200		kΩ
		$V_S = \pm 5V$, $V_{OUT} = \pm 2V$, $R_L = 10\Omega$	•	75	200		kΩ
V _{OUT}	Maximum Output Voltage Swing	$T_A = 25$ °C, $V_S = \pm 15$ V, $R_L = 10\Omega$ (Note 3)	•	±10.0 ±8.5	±11.5		V V
		$T_A = 25$ °C, $V_S = \pm 5$ V, $R_L = 10\Omega$	•	±2.5 ±2.0	±3.0		V V
I _{OUT}	Maximum Output Current (Note 4)	$V_S = \pm 15V$, $R_L = 1\Omega$	•	1.1	2.0		А
Is	Supply Current (Note 4)	$T_A = 25$ °C, $V_S = \pm 15$ V, $V_{SD} = 0$ V	•		35	50 65	mA mA
	Supply Current, R _{SD} = 51k (Notes 4, 5)	$T_A = 25$ °C, $V_S = \pm 15V$			15	30	mA
	Positive Supply Current, Shutdown	$V_S = \pm 15V, V_{SD} = 15V$	•			200	μА
	Output Leakage Current, Shutdown	$V_S = \pm 15V, V_{SD} = 15V$	•			10	μΑ
SR	Slew Rate (Note 6) Slew Rate (Note 4)	$T_A = 25$ °C, $A_V = 2$, $R_L = 400\Omega$ $T_A = 25$ °C, $A_V = 2$, $R_L = 10\Omega$		400	900 900		V/µs V/µs
	Differential Gain (Notes 4, 7)	$V_S = \pm 15V, R_F = 750\Omega, R_G = 750\Omega, R_L = 15\Omega$			0.3		%
	Differential Phase (Notes 4, 7)	$V_S = \pm 15V, R_F = 750\Omega, R_G = 750\Omega, R_L = 15\Omega$			0.1		DEG
BW	Small-Signal Bandwidth	$\begin{array}{l} A_V=2, V_S=\pm 15 V, Peaking \leq 1 dB, \\ R_F=R_G=680\Omega, R_L=100\Omega \end{array}$			55		MHz
		$\begin{array}{c} A_V=2,V_S=\pm 15V,Peaking\leq 1dB,\\ R_F=R_G=576\Omega,R_L=10\Omega \end{array}$			35		MHz

Note 1: Stresses beyond those listed under Absolute Maximum Ratings may cause permanent damage to the device. Exposure to any Absolute Maximum Rating condition for extended periods may affect device reliability and lifetime.

Note 2: Applies to short circuits to ground only. A short circuit between the output and either supply may permanently damage the part when operated on supplies greater than ± 10 V.

Note 3: Commercial grade parts are designed to operate over the temperature range of $-40^{\circ}\text{C} \leq \text{T}_{\text{A}} \leq 85^{\circ}\text{C}$, but are neither tested nor guaranteed beyond $0^{\circ}\text{C} \leq \text{T}_{\text{A}} \leq 70^{\circ}\text{C}$. Industrial grade parts tested over $-40^{\circ}\text{C} \leq \text{T}_{\text{A}} \leq 85^{\circ}\text{C}$ are available on special request. Consult factory.

Note 4: SO package is recommended for $\pm 5V$ supplies only, as the power dissipation of the SO package limits performance on higher supplies. For supply voltages greater than $\pm 5V$, use the TO-220 or DD package. See "Thermal Considerations" in the Applications Information section for details on calculating junction temperature. If the maximum dissipation of the package is exceeded, the device will go into thermal shutdown.

Note 5: R_{SD} is connected between the Shutdown pin and ground.

Note 6: Slew rate is measured at ± 5 V on a ± 10 V output signal while operating on ± 15 V supplies with R_F = 1.5k, R_G = 1.5k and R_L = 400Ω .

Note 7: NTSC composite video with an output level of 2V.



SMALL-SIGNAL BANDWIDTH

 ${\rm R}_{SD}$ = 0 $\!\Omega,~{\rm I}_{S}$ = 30mA, ${\rm V}_{S}$ = $\pm5 V,~{\rm Peaking} \leq 1 {\rm d}B$

A _V	RL	R _F	R _G	-3dB BW (MHz)
-1	150	549	549	52.5
	30	590	590	39.7
	10	619	619	26.5
1	150	604	-	53.5
	30	649	-	39.7
	10	619	-	27.4
2	150	562	562	51.8
	30	590	590	38.8
	10	576	576	27.4
10	150	392	43.2	48.4
	30	383	42.2	40.3
	10	215	23.7	36.0

 R_{SD} = 0 $\!\Omega,~I_{S}$ = 35mA, V_{S} = $\pm 15 V,~Peaking \leq 1 dB$

A _V	RL	R _F	R _G	-3dB BW (MHz)
-1	150	604	604	66.2
	30	649	649	48.4
	10	665	665	46.5
1	150	750	-	56.8
	30	866	-	35.4
	10	845	-	24.7
2	150	665	665	52.5
	30	715	715	38.9
	10	576	576	35.0
10	150	453	49.9	61.5
	30	432	47.5	43.1
	10	221	24.3	45.5

 R_{SD} = 7.5k, I_{S} = 15mA, V_{S} = $\pm 5V,$ Peaking $\leq 1 dB$

A _V	RL	R _F	R _G	-3dB BW (MHz)
-1	150	562	562	39.7
	30	619	619	28.9
	10	604	604	20.5
1	150	634	-	41.9
	30	681	-	29.7
	10	649	-	20.7
2	150	576	576	40.2
	30	604	604	29.6
	10	576	576	21.6
10	150	324	35.7	39.5
	30	324	35.7	32.3
	10	210	23.2	27.7

 R_{SD} = 47.5k, I_S = 18mA, V_S = $\pm 15 V, \, Peaking \leq 1 dB$

A _V	RL	R _F	R _G	-3dB BW (MHz)
-1	150	619	619	47.8
	30	698	698	32.3
	10	698	698	22.2
1	150	732	_	51.4
	30	806	_	33.9
	10	768	_	22.5
2	150	634	634	48.4
	30	698	698	33.0
	10	681	681	22.5
10	150	348	38.3	46.8
	30	357	39.2	36.7
	10	205	22.6	31.3

 R_{SD} = 15k, I_S = 7.5mA, V_S = $\pm 5 V, \, Peaking \leq 1 dB$

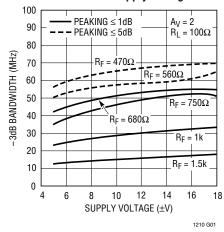
A _V	RL	R _F	R _G	-3dB BW (MHz)
-1	150	536	536	28.2
	30	549	549	20.0
	10	464	464	15.0
1	150	619	-	28.6
	30	634	-	19.8
	10	511	-	14.9
2	150	536	536	28.3
	30	549	549	19.9
	10	412	412	15.7
10	150	150	16.5	31.5
	30	118	13.0	27.1
	10	100	11.0	19.4

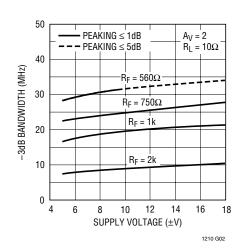
 R_{SD} = 82.5k, I_S = 9mA, V_S = $\pm 15 V, \ Peaking \leq 1 dB$

A _V	RL	R _F	R _G	-3dB BW (MHz)
-1	150	590	590	34.8
	30	649	649	22.5
	10	576	576	16.3
1	150	715	-	35.5
	30	768	-	22.5
	10	649	-	16.1
2	150	590	590	35.3
	30	665	665	22.5
	10	549	549	16.8
10	150	182	20.0	37.2
	30	182	20.0	28.9
	10	100	11.0	22.5

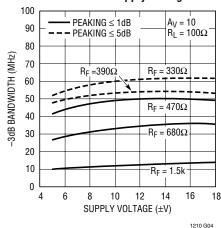
TYPICAL PERFORMANCE CHARACTERISTICS

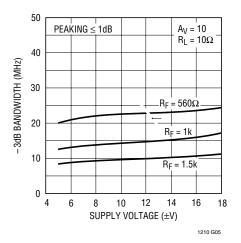
Bandwidth vs Supply Voltage





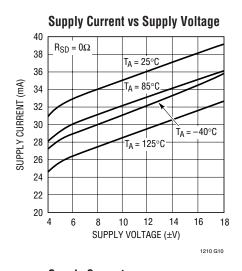
Bandwidth vs Supply Voltage

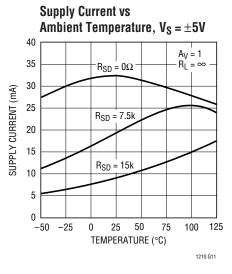


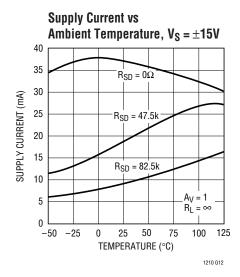


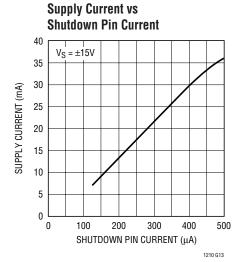


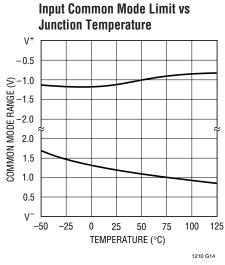
TYPICAL PERFORMANCE CHARACTERISTICS

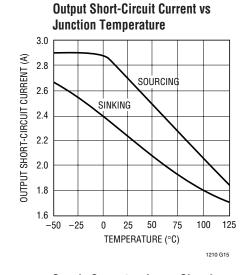


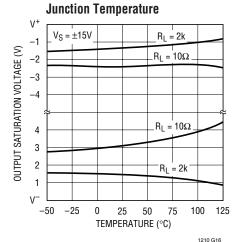




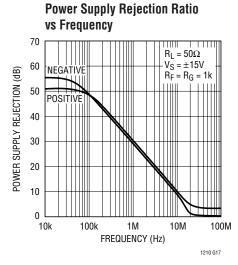


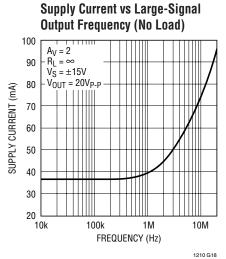




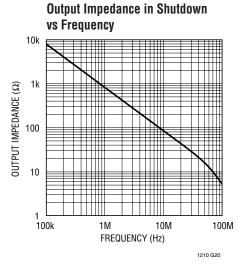


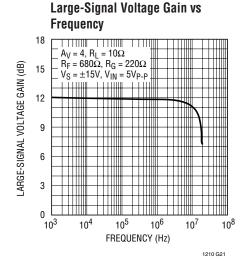
Output Saturation Voltage vs



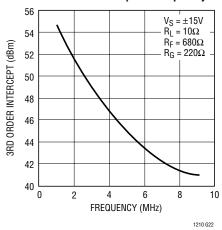


TYPICAL PERFORMANCE CHARACTERISTICS

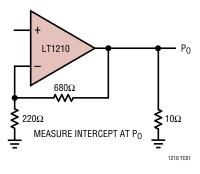




3rd Order Intercept vs Frequency



Test Circuit for 3rd Order Intercept





The LT1210 is a current feedback amplifier with high output current drive capability. The device is stable with large capacitive loads and can easily supply the high currents required by capacitive loads. The amplifier will drive low impedance loads such as cables with excellent linearity at high frequencies.

Feedback Resistor Selection

The optimum value for the feedback resistors is a function of the operating conditions of the device, the load impedance and the desired flatness of response. The Typical AC Performance tables give the values which result in less than 1dB of peaking for various resistive loads and operating conditions. If this level of flatness is not required, a higher bandwidth can be obtained by use of a lower feedback resistor. The characteristic curves of Bandwidth vs Supply Voltage indicate feedback resistors for peaking up to 5dB. These curves use a solid line when the response has 1dB to 5dB of peaking. The curves stop where the response has more than 5dB of peaking.

For resistive loads, the COMP pin should be left open (see Capacitive Loads section).

Capacitive Loads

The LT1210 includes an optional compensation network for driving capacitive loads. This network eliminates most of the output stage peaking associated with capacitive loads, allowing the frequency response to be flattened. Figure 1 shows the effect of the network on a 200pF load. Without the optional compensation, there is a 6dB peak at 40MHz caused by the effect of the capacitance on the output stage. Adding a 0.01µF bypass capacitor between the output and the COMP pins connects the compensation and greatly reduces the peaking. A lower value feedback resistor can now be used, resulting in a response which is flat to ± 1 dB to 40MHz. The network has the greatest effect for C_I in the range of OpF to 1000pF. The graphs of Bandwidth and Feedback Resistance vs Capacitive Load can be used to select the appropriate value of feedback resistor. The values shown are for 1dB and 5dB peaking at a gain of 2 with no resistive load. This is a worst-case condition, as the amplifier is more stable at higher gains and with some resistive load in parallel with the capaci-

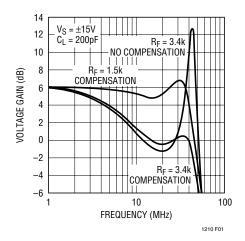


Figure 1

tance. Also shown is the -3dB bandwidth with the suggested feedback resistor vs the load capacitance.

Although the optional compensation works well with capacitive loads, it simply reduces the bandwidth when it is connected with resistive loads. For instance, with a 10Ω load, the bandwidth drops from 35MHz to 26MHz when the compensation is connected. Hence, the compensation was made optional. To disconnect the optional compensation, leave the COMP pin open.

Shutdown/Current Set

If the shutdown feature is not used, the SHUTDOWN pin must be connected to ground or V^- .

The Shutdown pin can be used to either turn off the biasing for the amplifier, reducing the quiescent current to less than $200\mu A$, or to control the quiescent current in normal operation.

The total bias current in the LT1210 is controlled by the current flowing out of the Shutdown pin. When the Shutdown pin is open or driven to the positive supply, the part is shut down. In the shutdown mode, the output looks like a 70pF capacitor and the supply current is typically less than 100 μA . The Shutdown pin is referenced to the positive supply through an internal bias circuit (see the Simplified Schematic). An easy way to force shutdown is to use open-drain (collector) logic. The circuit shown in Figure 2 uses a 74C904 buffer to interface between 5V logic and the LT1210. The switching time between the active and shutdown states is about $1\mu s$. A 24k pull-up resistor speeds



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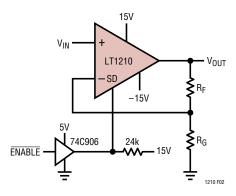


Figure 2. Shutdown Interface

up the turn-off time and ensures that the LT1210 is completely turned off. Because the pin is referenced to the positive supply, the logic used should have a breakdown voltage of greater than the positive supply voltage. No other circuitry is necessary as the internal circuit limits the Shutdown pin current to about $500\mu A$. Figure 3 shows the resulting waveforms.

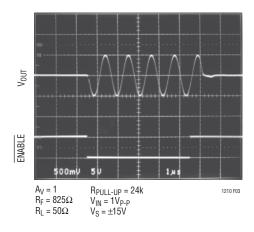


Figure 3. Shutdown Operation

For applications where the full bandwidth of the amplifier is not required, the quiescent current of the device may be reduced by connecting a resistor from the Shutdown pin to ground. The quiescent current will be approximately 65 times the current in the Shutdown pin. The voltage across the resistor in this condition is $V^+ - 3V_{BE}$. For example, a 82k resistor will set the quiescent supply current to 9mA with $V_S = \pm 15V$.

The photos in Figures 4a and 4b show the effect of reducing the quiescent supply current on the large-signal

response. The quiescent current can be reduced to 9mA in the inverting configuration without much change in response. In noninverting mode, however, the slew rate is reduced as the quiescent current is reduced.

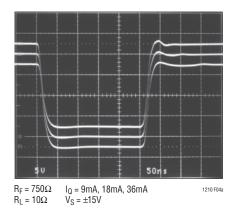


Figure 4a. Large-Signal Response vs I_0 , $A_V = -1$

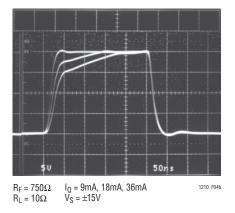


Figure 4b. Large-Signal Response vs I_Q , $A_V = 2$

Slew Rate

Unlike a traditional op amp, the slew rate of a current feedback amplifier is not independent of the amplifier gain configuration. There are slew rate limitations in both the input stage and the output stage. In the inverting mode, and for higher gains in the noninverting mode, the signal amplitude on the input pins is small and the overall slew rate is that of the output stage. The input stage slew rate is related to the quiescent current and will be reduced as the supply current is reduced. The output slew rate is set by the value of the feedback resistors and the internal capacitance. Larger feedback resistors will reduce the slew rate as will lower supply voltages, similar to the way



the bandwidth is reduced. The photos in Figures 5a, 5b and 5c show the large-signal response of the LT1210 for various gain configurations. The slew rate varies from $770V/\mu s$ for a gain of 1, to $1100V/\mu s$ for a gain of -1.

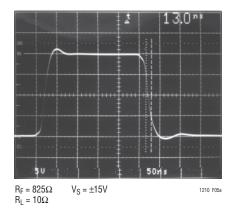


Figure 5a. Large-Signal Response, A_V = 1

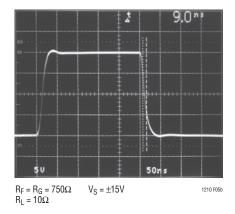


Figure 5b. Large-Signal Response, $A_V = -1$

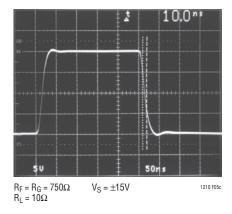


Figure 5c. Large-Signal Response, $A_V = 2$

When the LT1210 is used to drive capacitive loads, the available output current can limit the overall slew rate. In the fastest configuration, the LT1210 is capable of a slew rate of over 1V/ns. The current required to slew a capacitor at this rate is 1mA per picofarad of capacitance, so 10,000pF would require 10A! The photo (Figure 6) shows the large-signal behavior with $C_L = 10,000pF$. The slew rate is about 150V/ μ s, determined by the current limit of 1.5A.

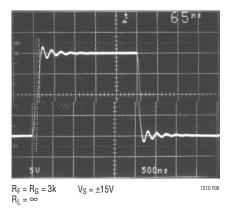


Figure 6. Large-Signal Response, C_L = 10,000pF

Differential Input Signal Swing

The differential input swing is limited to about $\pm 6V$ by an ESD protection device connected between the inputs. In normal operation, the differential voltage between the input pins is small, so this clamp has no effect; however, in the shutdown mode the differential swing can be the same as the input swing. The clamp voltage will then set the maximum allowable input voltage. To allow for some margin, it is recommended that the input signal be less than $\pm 5V$ when the device is shut down.

Capacitance on the Inverting Input

Current feedback amplifiers require resistive feedback from the output to the inverting input for stable operation. Take care to minimize the stray capacitance between the output and the inverting input. Capacitance on the inverting input to ground will cause peaking in the frequency response (and overshoot in the transient response), but it does not degrade the stability of the amplifier.





T7 Package, 7-Lead T0-220

Thermal Resistance (Junction-to-Case) = 5°C/W

Calculating Junction Temperature

The junction temperature can be calculated from the equation:

$$T_{II} = (P_D)(\theta_{IIA}) + T_A$$

where:

 T_J = Junction Temperature

T_A = Ambient Temperature

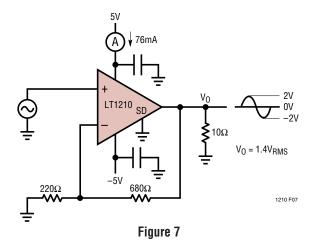
P_D = Device Dissipation

 θ_{JA} = Thermal Resistance (Junction-to-Ambient)

As an example, calculate the junction temperature for the circuit in Figure 7 for the SO and R packages assuming a 70°C ambient temperature.

The device dissipation can be found by measuring the supply currents, calculating the total dissipation and then subtracting the dissipation in the load and feedback network.

$$P_D = (76\text{mA})(10\text{V}) - (1.4\text{V})^2 / 10 = 0.56\text{W}$$



then:

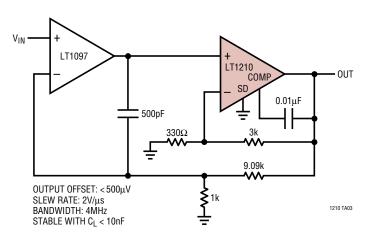
 $T_J = (0.56W)(46^{\circ}C/W) + 70^{\circ}C = 96^{\circ}C$ for the SO package with 1000 sq. mm topside heat sinking

 $T_J = (0.56W)(27^{\circ}C/W) + 70^{\circ}C = 85^{\circ}C$ for the R package with 1000 sq. mm topside heat sinking

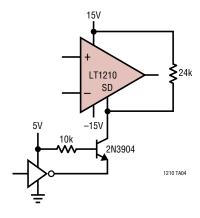
Since the maximum junction temperature is 150°C, both packages are clearly acceptable.

TYPICAL APPLICATIONS

Precision ×10 High Current Amplifier



CMOS Logic to Shutdown Interface

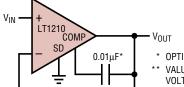


NEAD

TYPICAL APPLICATIONS

Distribution Amplifier

Buffer $A_V = 1$

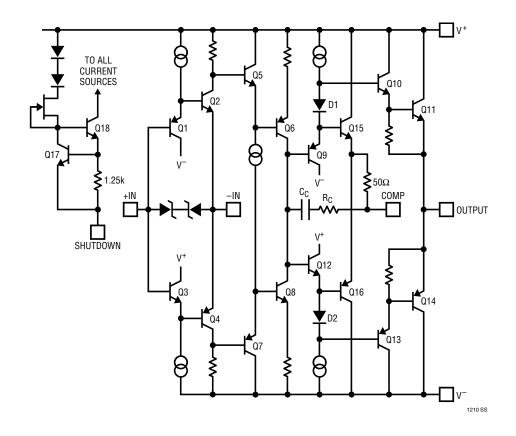


* OPTIONAL, USE WITH CAPACITIVE LOADS

** VALUE OF R_F DEPENDS ON SUPPLY
VOLTAGE AND LOADING. SELECT
FROM TYPICAL AC PERFORMANCE

TABLE OR DETERMINE EMPIRICALLY

SIMPLIFIED SCHEMATIC

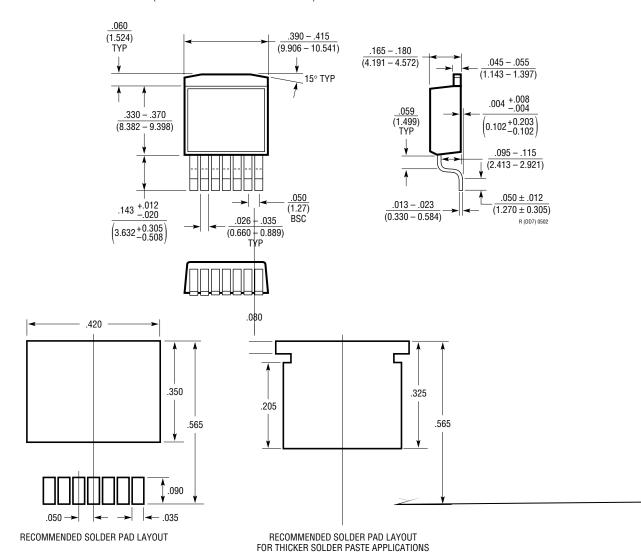




PACKAGE DESCRIPTION

R Package 7-Lead Plastic DD Pak

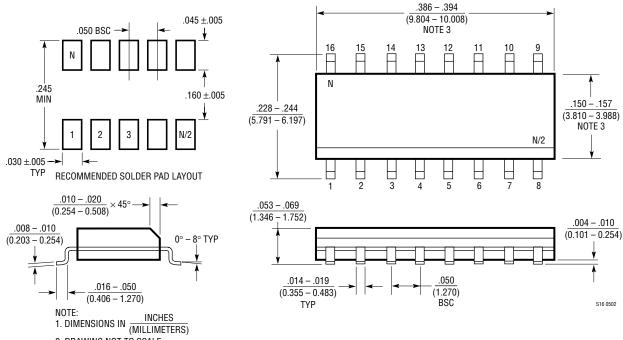
(Reference LTC DWG # 05-08-1462)



PACKAGE DESCRIPTION

S Package 16-Lead Plastic Small Outline (Narrow .150 Inch)

(Reference LTC DWG # 05-08-1610)

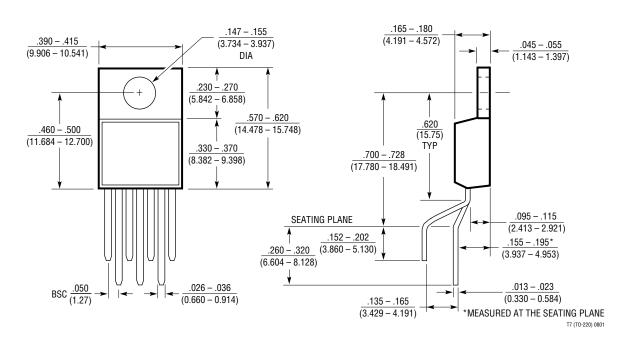


2. DRAWING NOT TO SCALE

3. THESE DIMENSIONS DO NOT INCLUDE MOLD FLASH OR PROTRUSIONS.
MOLD FLASH OR PROTRUSIONS SHALL NOT EXCEED .006" (0.15mm)

T7 Package 7-Lead Plastic TO-220 (Standard)

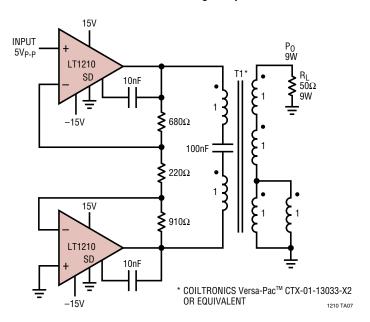
(Reference LTC DWG # 05-08-1422)



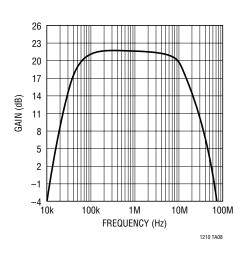


TYPICAL APPLICATION

Wideband 9W Bridge Amplifier



Frequency Response



RELATED PARTS

PART NUMBER	DESCRIPTION	COMMENTS		
LT1010	Fast ±150mA Power Buffer	20MHz Bandwidth, 75V/µs Slew Rate		
LT1166	Power Output Stage Automatic Bias System	Sets Class AB Bias Currents for High Voltage/High Power Output Stages		
LT1206 Single 250mA, 60MHz Current Feedback Amplifier		Shutdown Function, Stable with C_L = 10,000pF, 900V/ μ s Slew Rate		
LT1207	Dual 250mA, 60MHz Current Feedback Amplifier	Dual Version of LT1206		
LT1227	Single 140MHz Current Feedback Amplifier	Shutdown Function, 1100V/µs Slew Rate		
LT1360	Single 50MHz, 800V/ μ s Op Amp Voltage Feedback, Stable with $C_L = 10,000$ pF			
LT1363	Single 70MHz, 1000V/ μ s Op Amp Voltage Feedback, Stable with $C_L = 10,000$ pF			